

Spring, 2022

ME 597 – Solid Mechanics II

Lecture 9

Hyperelastic solids

Stability and linearized equations

KEEP A MASK WITH
YOU AT ALL TIMES



**PROTECT
PURDUE**



Mechanical Engineering

Instructor: Prof. Marcial Gonzalez

Last modified: 2/8/22 7:55:17 PM

Hyperelastic solids - Isotropic

Review: Incompressible hyperelastic materials

$$W(\lambda_1, \lambda_2, \lambda_3) = \sum_{p=1}^N \frac{\mu_p}{\alpha_p} (\lambda_1^{\alpha_p} + \lambda_2^{\alpha_p} + \lambda_3^{\alpha_p} - 3) \quad \text{Ogden model}$$

Limit of infinitesimal deformations: $\mu = \frac{1}{2} \sum_{p=1}^N \mu_p \alpha_p$ with $\mu_p \alpha_p > 0$
shear modulus

$$W(I_1, I_2) = c_1(I_1 - 3) + c_2(I_2 - 3) \quad \text{Mooney-Rivlin materials}$$

$$W(I_1, I_2) = c_1(I_1 - 3) \quad \text{neo-Hookean materials}$$

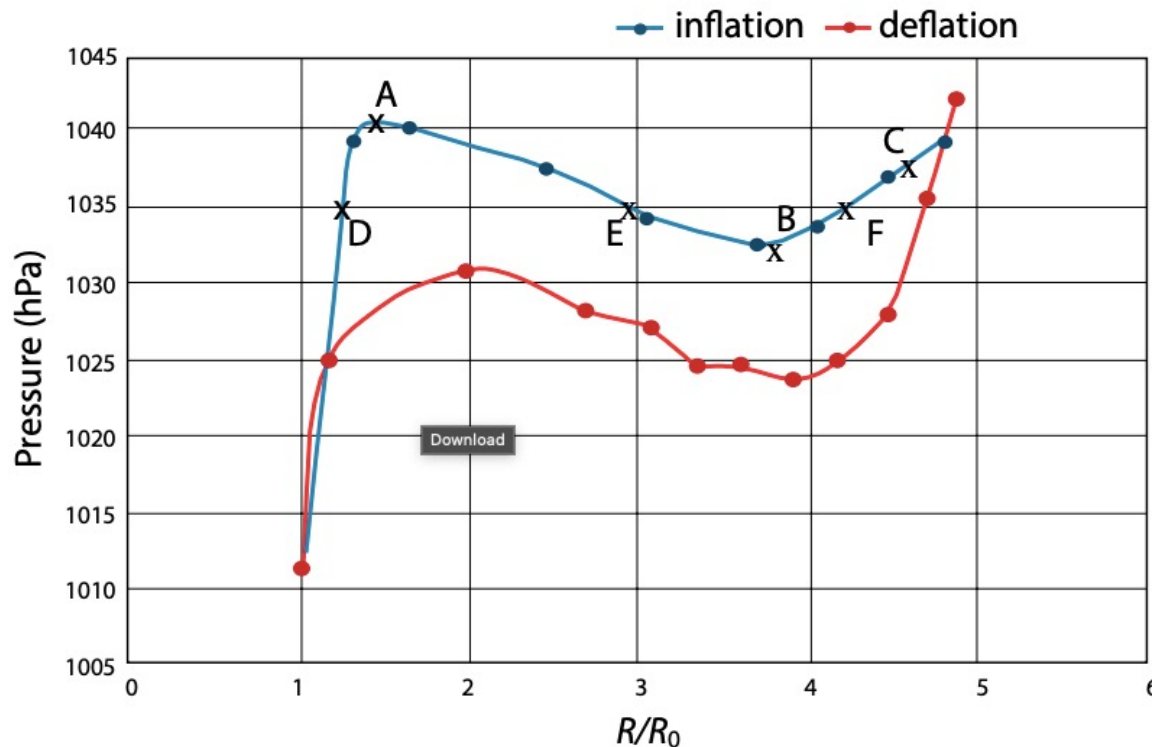
Limit of infinitesimal deformations: $\mu = 2(c_1 + c_2)$ $E = 6(c_1 + c_2)$
shear modulus Young's modulus

Note: incompressibility is an internal constraint (or kinematic constraint) of the material $\lambda_3 = 1/\lambda_1\lambda_2$ $I_3 = 1$

Note: Pressure is introduced as a Lagrange multiplier and determined from boundary conditions.

Hyperelastic solids - Isotropic

Inflation of a spherical (incompressible rubber) balloon



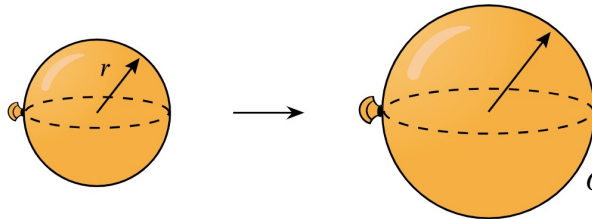
"It has been reposted [...] that smartphone barometers are good enough for real physics experiments"

Source: Julien Vandermarlière, "On the inflation of a rubber balloon"
The Physics Teacher 54, 566-567 (2016)

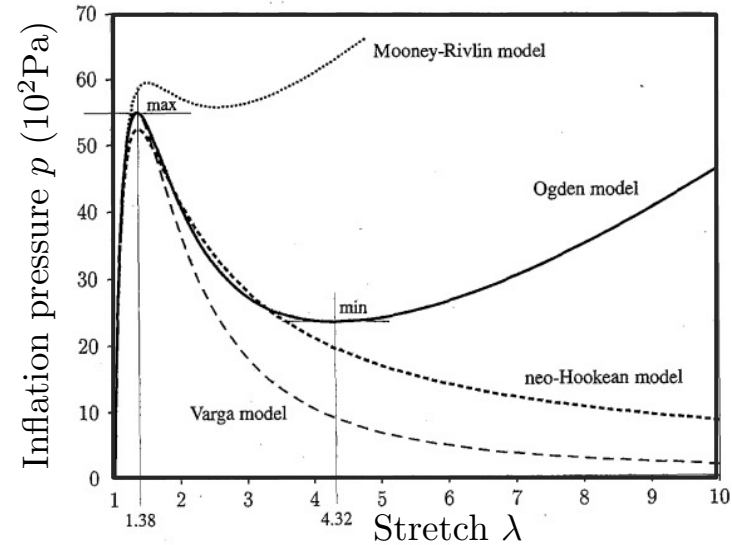
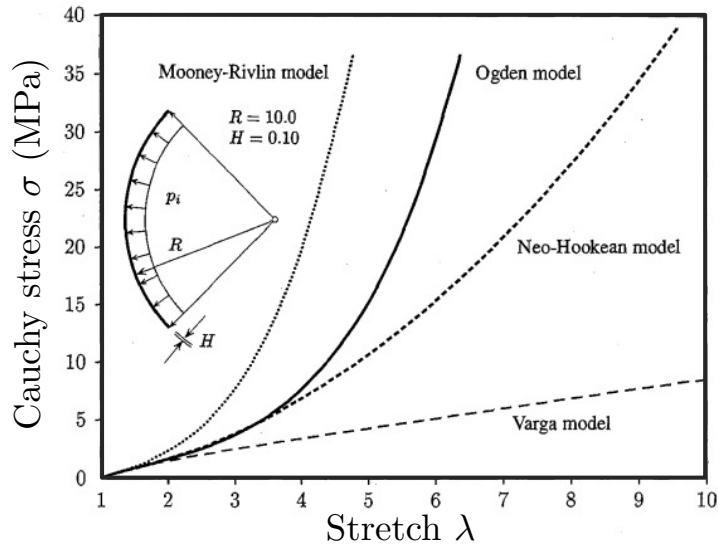
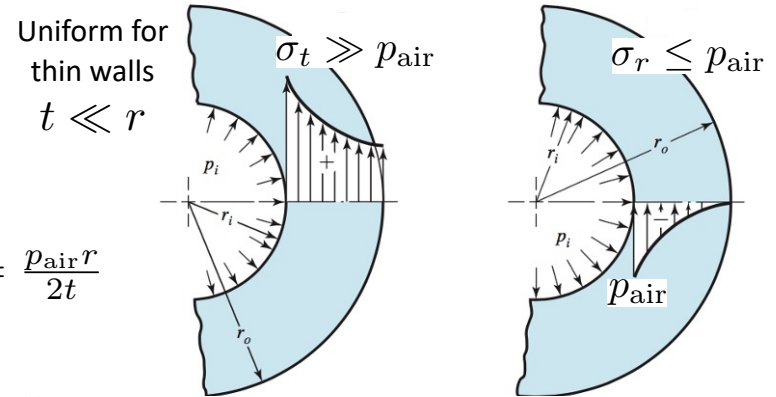
Hyperelastic solids - Isotropic

Inflation of a spherical (incompressible rubber) balloon

Spherical inflation mode $\lambda_1 = \lambda_2 = \frac{r}{R}$



$$\sigma_{11} = \sigma_{22} = \frac{p_{\text{air}} r}{2t}$$

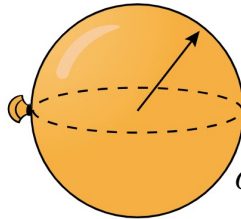
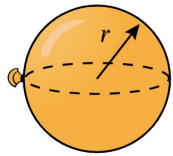


Source: Harold Alexander, "Tensile instability of initially spherical balloons", Int. J. Engng Sci. Vol. 9, 151-162, 1971.

Hyperelastic solids - Isotropic

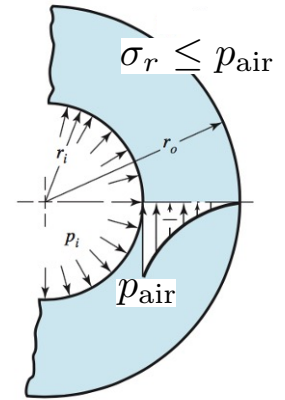
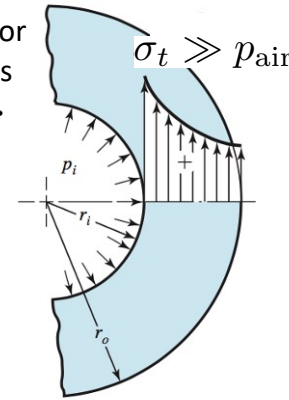
Inflation of a spherical (incompressible rubber) balloon

Spherical inflation mode $\lambda_1 = \lambda_2 = \frac{r}{R}$



$$\sigma_{11} = \sigma_{22} = \frac{p_{\text{air}} r}{2t}$$

Uniform for thin walls
 $t \ll r$

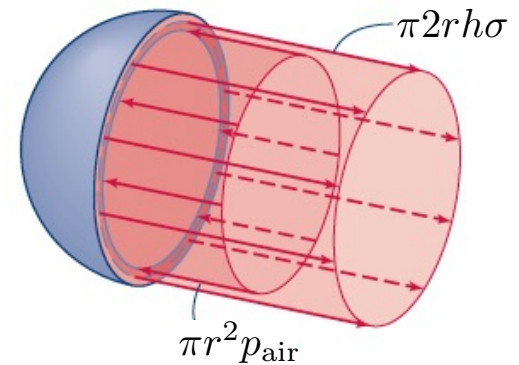
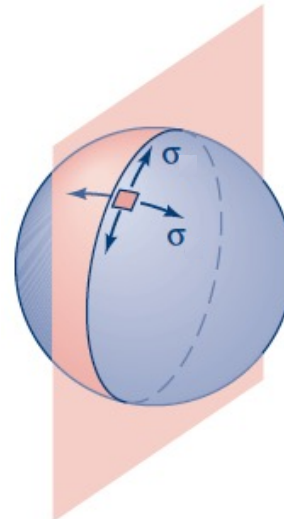
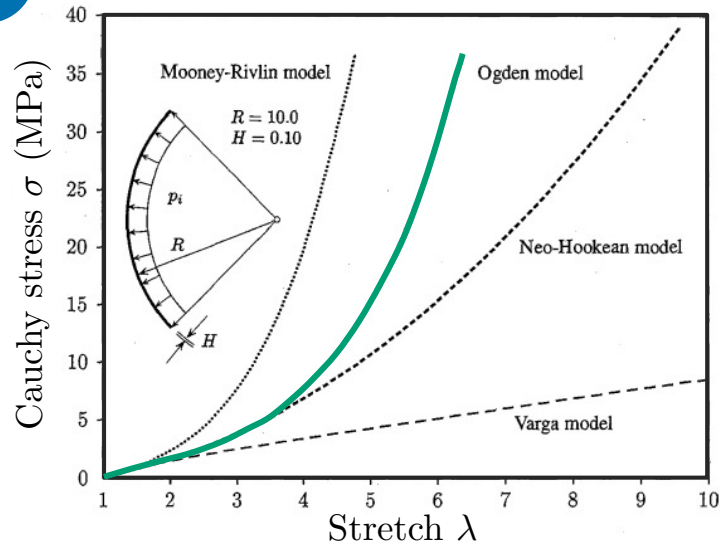


DIY

Hyperelastic solids - Isotropic

Inflation of a spherical (incompressible rubber) balloon

DIY



Source: Holzapfel G.A., "Nonlinear Solid Mechanics", Wiley, 2000.

Hyperelastic solids - Isotropic

Inflation of a spherical (incompressible rubber) balloon

DIY

Questions ...

How is the experiment carried out?

Is it a load-controlled or a displacement-controlled experiment?

What is a (stable) equilibrium configuration?

$$\alpha_1 = 1.3$$

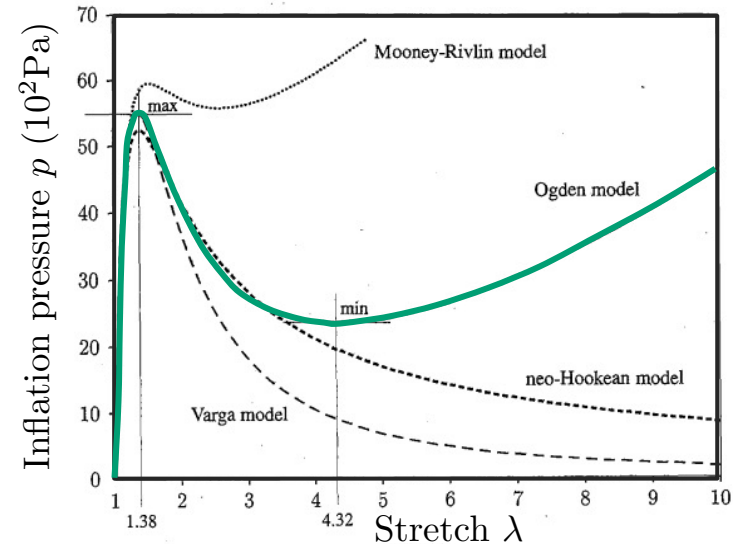
$$\alpha_2 = 5.0$$

$$\alpha_3 = -2.0$$

$$\mu_1 = 6.3 \cdot 10^5 \text{N/m}^2$$

$$\mu_2 = 0.012 \cdot 10^5 \text{N/m}^2$$

$$\mu_3 = -0.1 \cdot 10^5 \text{N/m}^2$$



Stability of hyperelastic solids

Static equilibrium – Stability

- Principle of stationary potential energy:

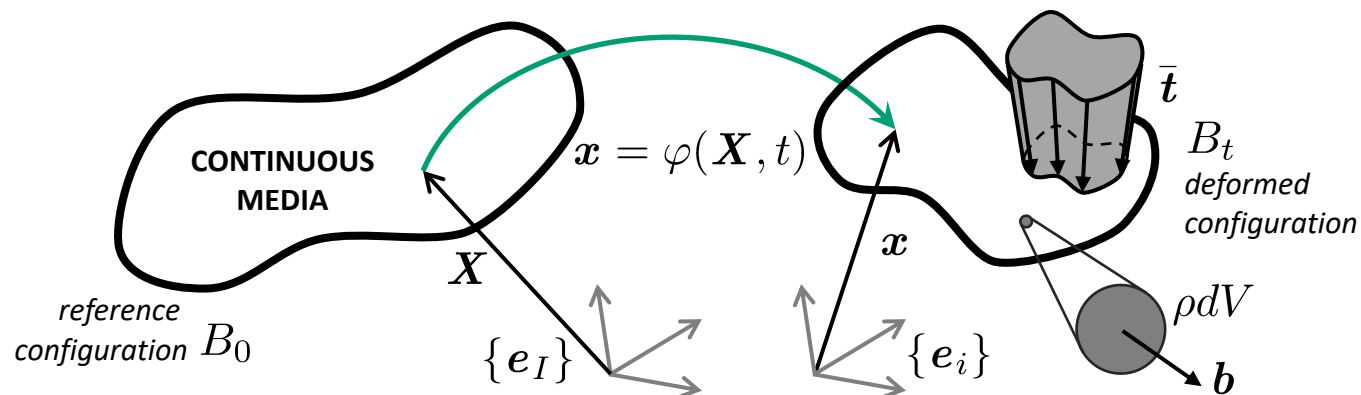
Given the set of admissible displacement fields for a conservative system, an equilibrium state will correspond to one for which the potential energy is stationary

$$\Pi = \int_{B_0} W(\mathbf{F}) dV_0 - \int_{B_0} \rho \mathbf{b} \cdot \boldsymbol{\varphi} dV_0 - \int_{\partial B_0} \mathbf{t} \cdot \boldsymbol{\varphi} dA_0$$

—— internal ——
—— external ——

- Stable solution?

A stationary point could be a minimum, a maximum or a saddle point.

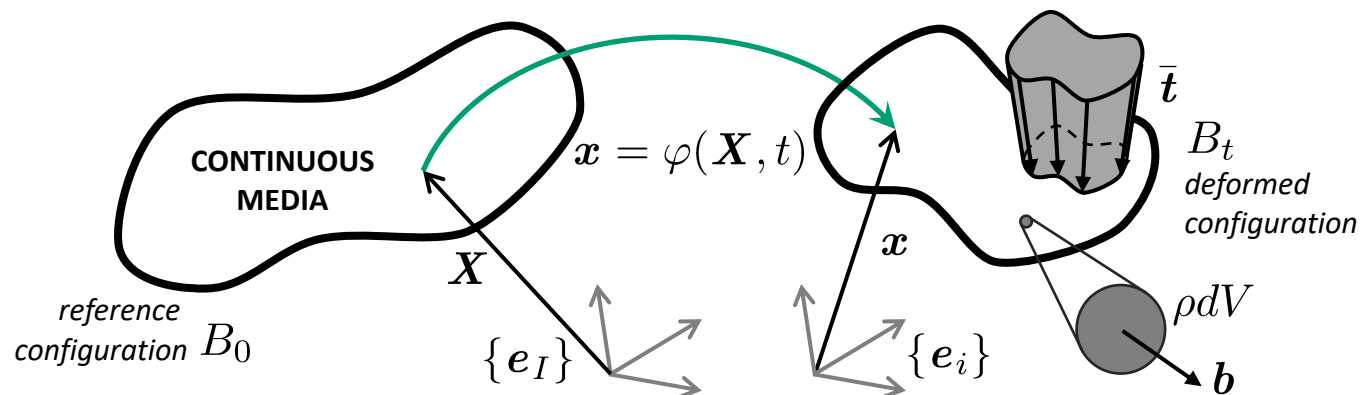


Stability of hyperelastic solids

Static equilibrium – Stability

- Stable solution?
A stationary point could be a minimum, a maximum or a saddle point.
- Theory of stability of infinite-dimensional spaces is not trivial ...

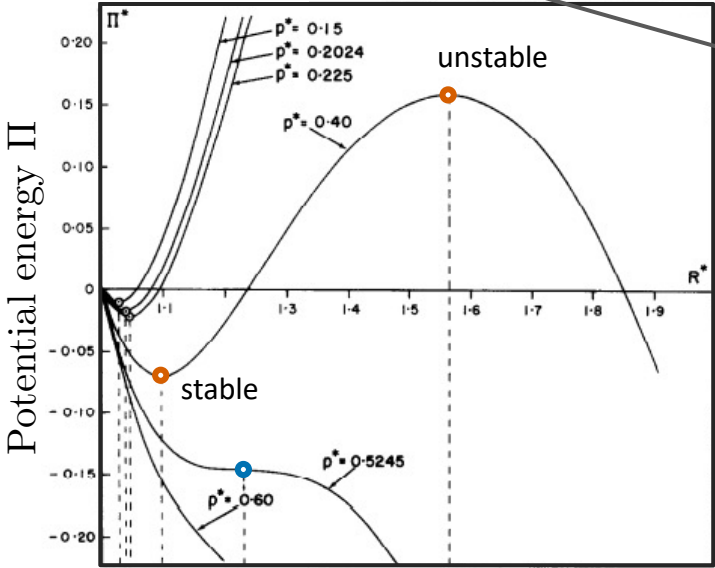
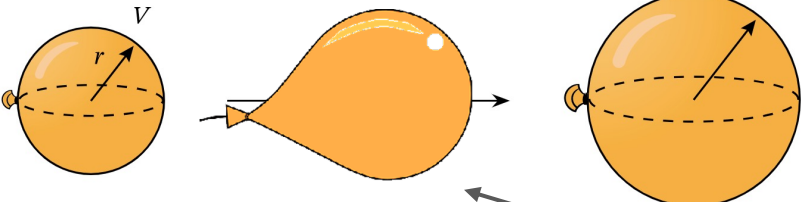
.... but, ultimately, *necessary conditions* can be inferred from the strain energy density, and *sufficient conditions* come from nonlinear terms (e.g., in the deformation mapping) and from boundary conditions.



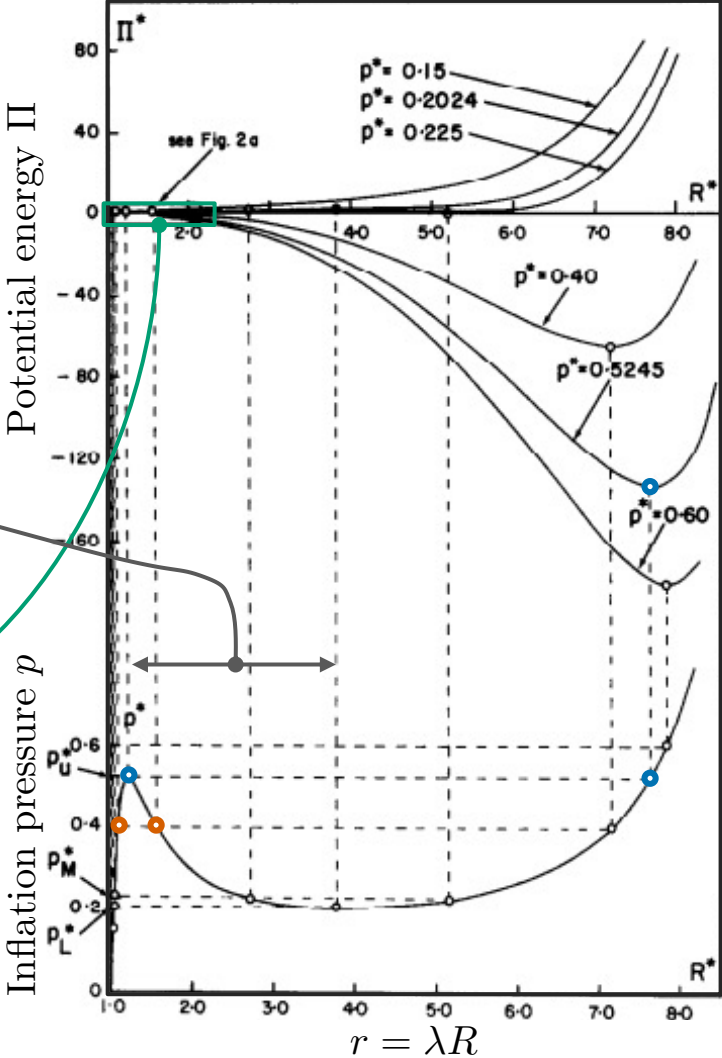
Stability of hyperelastic solids

Inflation of a spherical balloon

Spherical inflation mode $\lambda_1 = \lambda_2 = \frac{r}{R}$



$$r = \lambda R$$



Source: Harold Alexander, "Tensile instability of initially spherical balloons", Int. J. Engng Sci. Vol. 9, 151-162, 1971.

Linearized constitutive equations

Review: Linearized kinematics

- Linearized or incremental expressions for the kinematic quantities are required when:

(i) the deformation process is described as a series of small steps

$$\boldsymbol{x} = \boldsymbol{\varphi}(\boldsymbol{X}) \rightarrow \boldsymbol{\varphi}(\boldsymbol{X}) + \boldsymbol{u}(\boldsymbol{X})$$

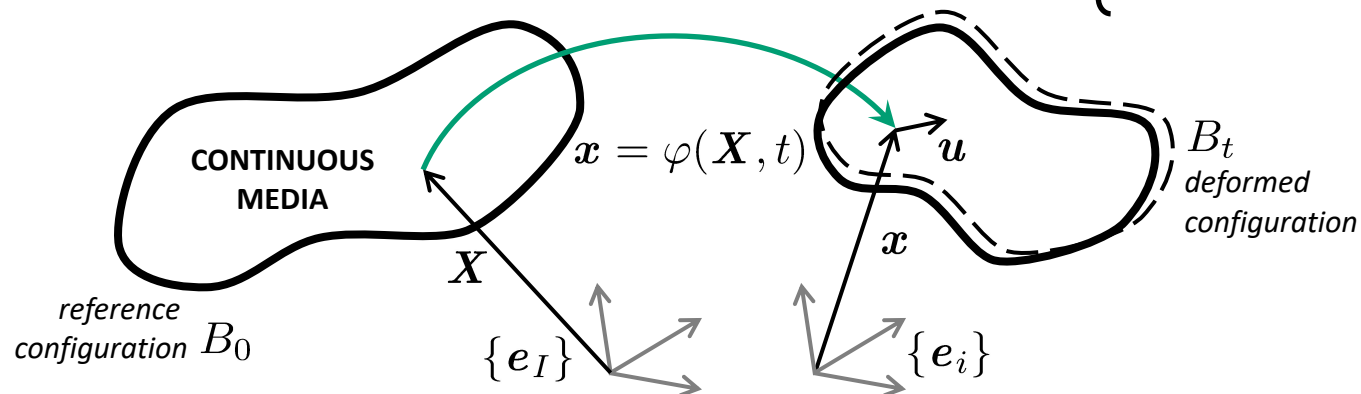
(ii) displacements are indeed small

$$\boldsymbol{X} \rightarrow \boldsymbol{X} + \boldsymbol{u}(\boldsymbol{X})$$

- If the linearization is evaluated in the 'stress free' undeformed configuration ($\boldsymbol{F}^* = \boldsymbol{I}$, $J^* = 1$, $\boldsymbol{\sigma} = \mathbf{0}$), then

$$\boldsymbol{S} = \mathbb{C} : \boldsymbol{E} \rightarrow d\boldsymbol{S}^* = \mathbb{C}^* : d\boldsymbol{E}^*$$

$$\left\{ \begin{array}{l} d\boldsymbol{E}^* = d\boldsymbol{\epsilon} \rightarrow \boldsymbol{\epsilon} \\ d\boldsymbol{S}^* = d\boldsymbol{\sigma} \rightarrow \boldsymbol{\sigma} \\ \mathbb{C}^* = \boldsymbol{c} \end{array} \right.$$



Linearized constitutive equations

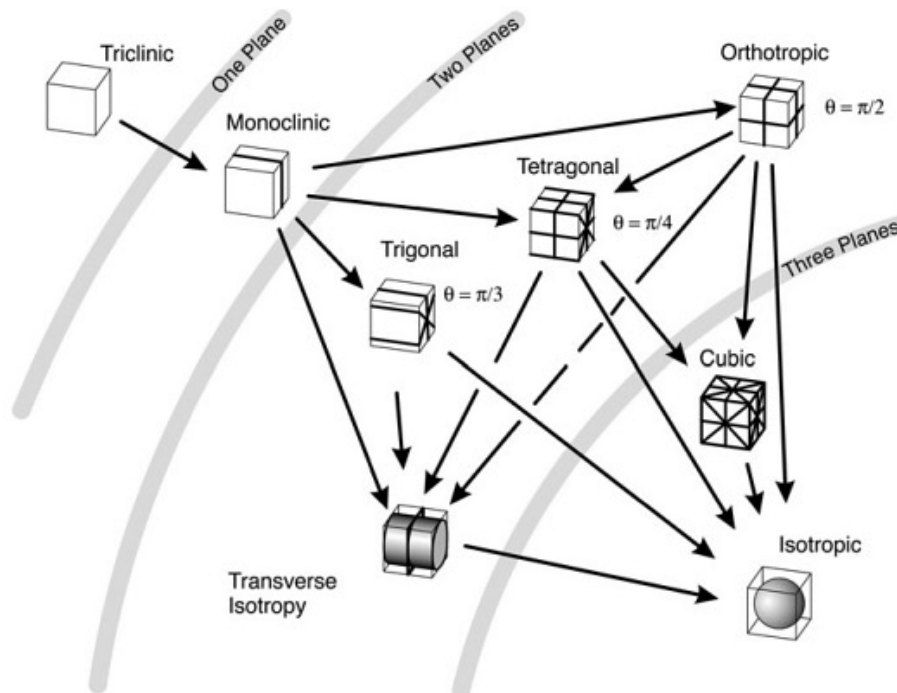
Generalized Hooke's law as a linearized hyperelasticity

- Material symmetry

$$\sigma_{ij} = C_{ijkl}\epsilon_{kl} \iff \boldsymbol{\sigma} = \mathbf{C} : \boldsymbol{\epsilon} \quad \text{(small strain) elasticity tensor}$$

(minor and major symmetries)

$$C_{ijkl} = Q_{ip}Q_{jq}Q_{kr}Q_{ls}C_{pqrs} \quad \forall \mathbf{Q} = \mathbf{H} \in G \subset SO(3)$$



Symmetry Classes	Point Group	Symmetry Operation
Triclinic	1	One onefold
Monoclinic	2	One twofold
Orthotropic	222	Three twofold
Tetragonal	4	One fourfold
Trigonal	3	One threefold
Transv. Isotropy	6	One sixfold
Cubic	23	Four threefold
Isotropic	-	

Linearized constitutive equations

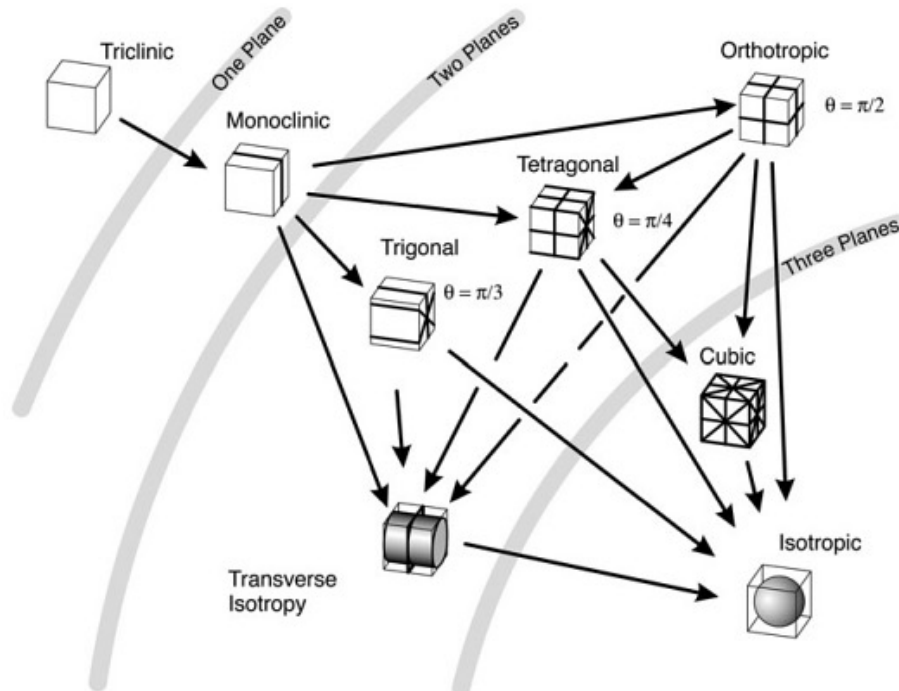
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Note:

Symmetries are retained only under small deformations.

Although any symmetry can be cast into an incremental formulation, it might not result in an accurate representation.

Linearized constitutive equations

Generalized Hooke's law as a linearized hyperelasticity

- Material symmetry: isotropic material

$$\sigma_{ij} = C_{ijkl}\epsilon_{kl} \iff \boldsymbol{\sigma} = \mathbf{C} : \boldsymbol{\epsilon} \quad \text{(small strain) elasticity tensor}$$

(minor and major symmetries)

$$C_{ijkl} = Q_{ip}Q_{jq}Q_{kr}Q_{ls}C_{pqrs} \quad \forall \mathbf{Q} \in G \subset SO(3)$$

Isotropic (any proper rotation) $\mathbf{Q} = \mathbf{R}^T \in SO(3)$

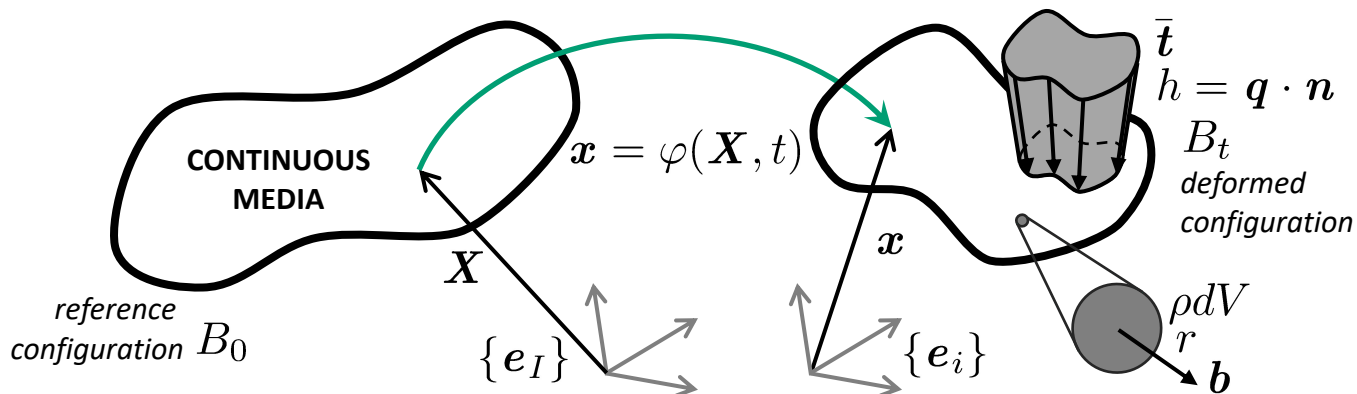
$$C_{ijkl} = \lambda \delta_{ij}\delta_{kl} + \mu(\delta_{ik}\delta_{jl} + \delta_{il}\delta_{jk})$$

$$\lambda = c_{1122} = c_{1133} = c_{2211}$$

$$c_{1111} = c_{2222} = c_{3333}$$

$$\mu = c_{2323} = (c_{1111} - c_{1122})/2 = c_{1313} = c_{1212}$$

DIY



Linearized constitutive equations

Generalized Hooke's law as a linearized hyperelasticity

- Material symmetry: isotropic material

$$\sigma_{ij} = C_{ijkl}\epsilon_{kl} \iff \boldsymbol{\sigma} = \mathbf{C} : \boldsymbol{\epsilon} \quad \text{(small strain) elasticity tensor}$$

(minor and major symmetries)

$$C_{ijkl} = Q_{ip}Q_{jq}Q_{kr}Q_{ls}C_{pqrs} \quad \forall \mathbf{Q} \in G \subset SO(3)$$

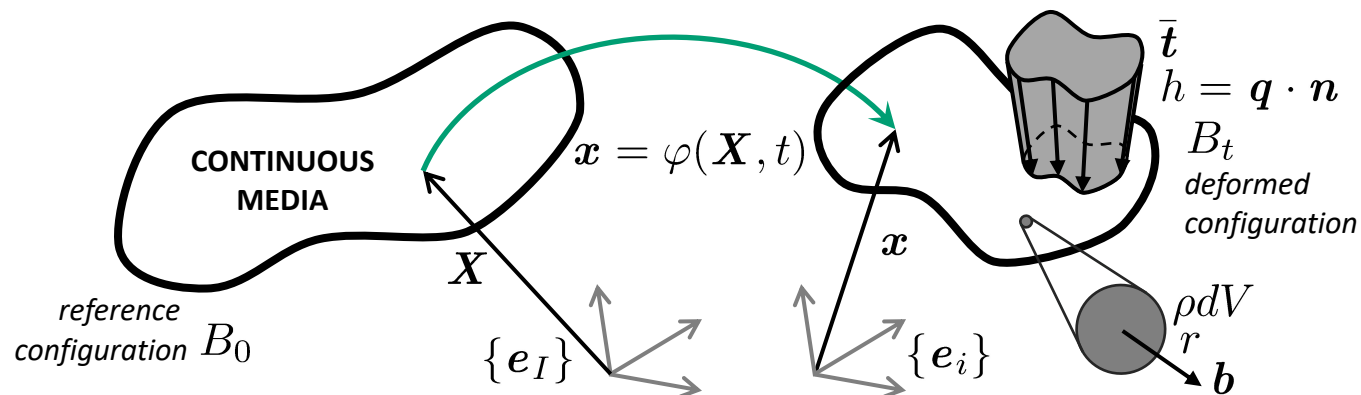
Isotropic (any proper rotation)

$$\mathbf{Q} = \mathbf{R}^T \in SO(3)$$

DIY

$$\boldsymbol{\sigma} = \lambda(\text{tr}\boldsymbol{\epsilon})\mathbf{I} + 2\mu\boldsymbol{\epsilon}$$

$$\boldsymbol{\epsilon} = -\frac{\nu}{E}(\text{tr}\boldsymbol{\sigma})\mathbf{I} + \frac{1+\nu}{E}\boldsymbol{\sigma}$$



Lecture 9 – Stability and linearized equations

Any questions?