

Spring, 2022

ME 597 – Solid Mechanics II

Lecture 11 Viscoelastic solids

KEEP A MASK WITH
YOU AT ALL TIMES



**PROTECT
PURDUE**

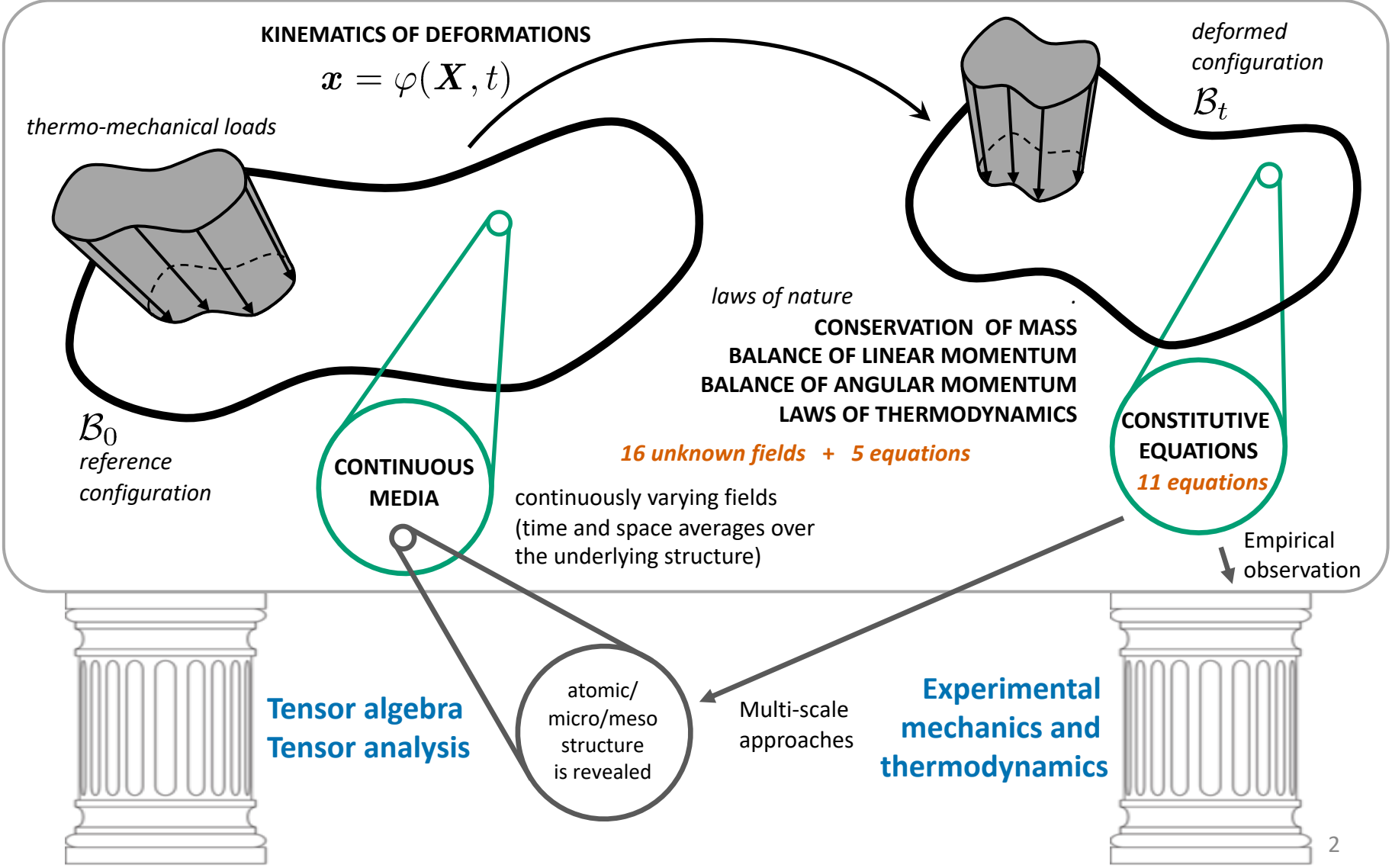


Mechanical Engineering

Instructor: Prof. Marcial Gonzalez

Last modified: 2/14/22 11:26:13 PM

Lecture 11 – Constitutive relations



Constitutive relations

Constraints on constitutive relations

- Relations that describe the response of the material to mechanical and thermal loading, e.g., $\boldsymbol{\sigma}, \mathbf{q}, u, T$ (11 constitutive equations)

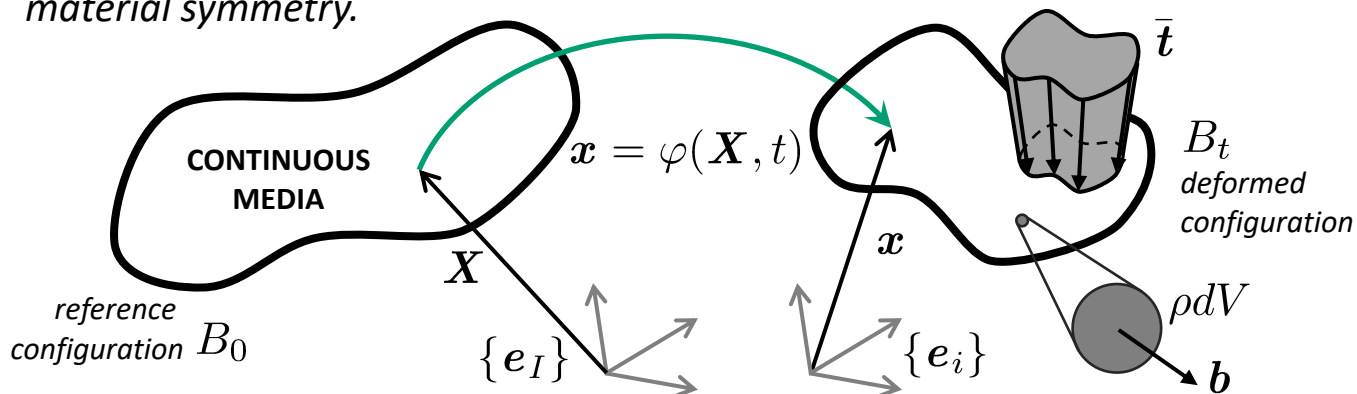
$$\boldsymbol{\sigma} = \boldsymbol{\sigma}^{(e)} + \boldsymbol{\sigma}^{(v)}, \mathbf{q} = \mathbf{0}, \rho_0 u(\mathbf{F}, s), \dot{T} \neq 0 \quad (\text{with } \dot{s} = 0) \quad \text{isothermal processes}$$

$$\boldsymbol{\sigma} = \boldsymbol{\sigma}^{(e)} + \boldsymbol{\sigma}^{(v)}, \mathbf{q} = \mathbf{0}, W(\mathbf{F}, T), \dot{s} \neq 0 \quad (\text{with } \dot{T} = 0) \quad \text{isentropic processes}$$

- Can these constitutive relations be selected arbitrarily? NO!

They must follow the following fundamental principles:

Principle of determinism, principle of local action, second law of thermodynamics restrictions (Clausius-Duhem inequality), principle of material frame indifference, material symmetry.



Constitutive relations

Constraints on constitutive relations

- Principle of determinism & Principle of local action

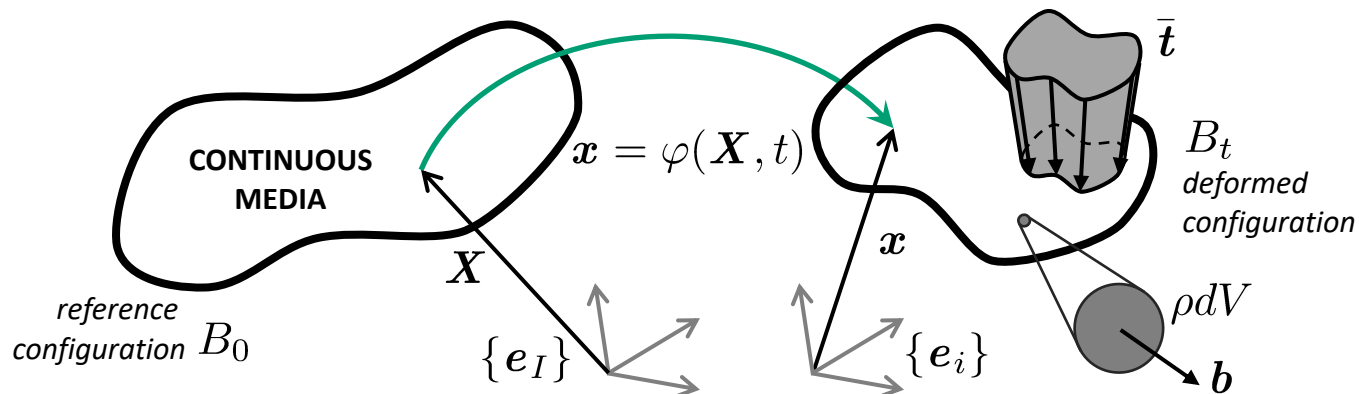
$$\boldsymbol{\sigma}(\mathbf{X}, t) = \mathbf{f}(\varphi^t, \mathbf{F}^t, \dots, \mathbf{T}^t, \nabla_0 \mathbf{T}^t, \dots, \mathbf{X}, t)$$

time series \square^t materials with memory

$\mathbf{f}(\dots, t)$ materials with aging




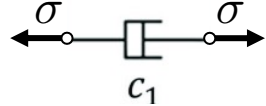


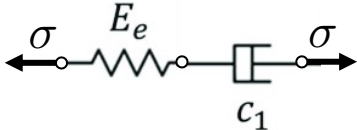


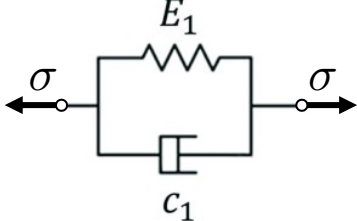


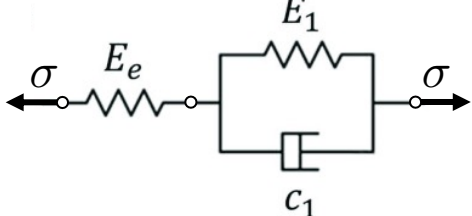


Simple elastic material $W = \bar{W}(\mathbf{C}, T)$ $\mathbf{S}^{(e)} = 2 \frac{\partial \bar{W}(\mathbf{C}, T)}{\partial \mathbf{C}}$ $\boldsymbol{\sigma}^{(v)}(\mathbf{C}, T, \mathbf{d})$
— simple fluids —

Material with memory (infinitesimal strain) $\boldsymbol{\sigma}(t) = \int_{-\infty}^t G(t - t') \dot{\boldsymbol{\epsilon}}(t') dt'$



Materials with memory

Creep, relaxation and hysteresis

		Creep	Relaxation	Model Parameters
Spring				1
Dashpot				1
Maxwell model				2
Kelvin/Voigt model				2
Standard linear model				3

Materials with memory

Wave propagation

- 1D viscoelastic solid
(balance of linear momentum) $\frac{\partial \sigma}{\partial x} = \rho \frac{\partial^2 u}{\partial t^2}$ $u(x, t) = u_0 e^{i(\omega t - kx)}$
 $\epsilon = \frac{\partial u}{\partial x}$ **complex wavenumber** k
frequency ω
- Standard linear model $\sigma + \frac{\eta_1}{E_0 + E_1} \dot{\sigma} = \frac{E_0 E_1}{E_0 + E_1} \left[\epsilon + \frac{\eta_1}{E_1} \dot{\epsilon} \right]$ **stress-strain-time**
- Fourier transform $\hat{\sigma}(\omega) = M(\omega) \hat{\epsilon}(\omega)$ $M(\omega)$ **complex modulus**

DIY

(cont.)

Materials with memory

Wave propagation

- 1D viscoelastic solid
(balance of linear momentum) $\frac{\partial \sigma}{\partial x} = \rho \frac{\partial^2 u}{\partial t^2}$ $u(x, t) = u_0 e^{i(\omega t - kx)}$
 $\epsilon = \frac{\partial u}{\partial x}$ **complex wavenumber** k
frequency ω
- Standard linear model $\sigma + \frac{\eta_1}{E_0 + E_1} \dot{\sigma} = \frac{E_0 E_1}{E_0 + E_1} \left[\epsilon + \frac{\eta_1}{E_1} \dot{\epsilon} \right]$ **stress-strain-time**
- Fourier transform $\hat{\sigma}(\omega) = M(\omega) \hat{\epsilon}(\omega)$ $M(\omega)$ **complex modulus**

$$M(\omega) = \dots$$

DIY

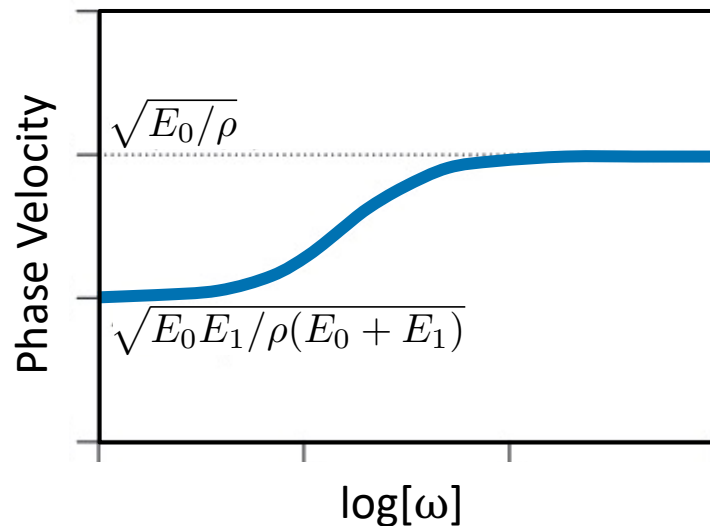
Materials with memory

Wave propagation – Phase velocity – Dispersion

- 1D viscoelastic solid (frequency domain) $Mk^2 = \omega^2 \rho$ **dispersion relation**

complex velocity $v_c(\omega) = \sqrt{\frac{M(\omega)}{\rho}} = \frac{\omega}{k}$

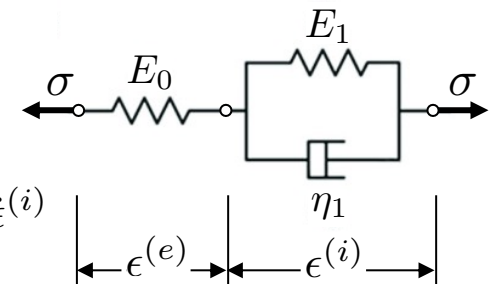
phase velocity $v_p(\omega) = [\text{Re}(1/v_c)]^{-1}$



$$\epsilon = \epsilon^{(e)} + \epsilon^{(i)}$$

$$\sigma = E_0 \epsilon^{(e)}$$

$$\sigma = E_1 \epsilon^{(i)} + \eta_1 \dot{\epsilon}^{(i)}$$

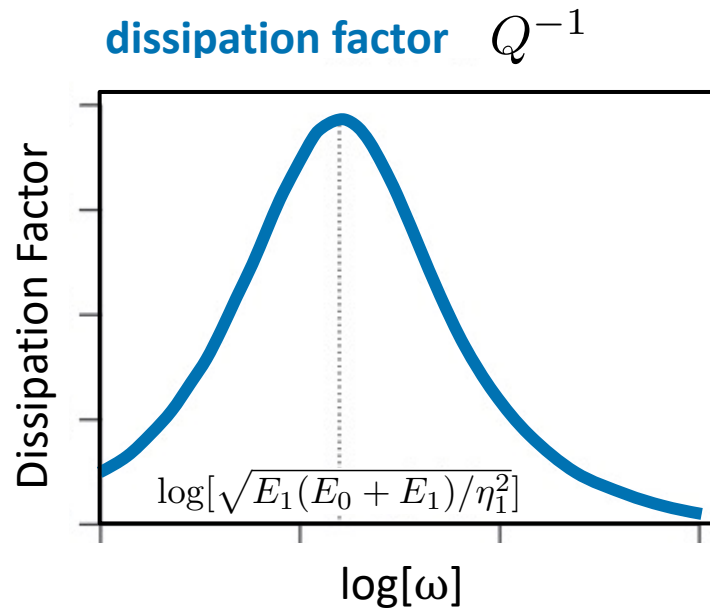


Materials with memory

Wave propagation – Dissipation

- Quality factor: twice the time-averaged strain-energy density divided by the time-averaged dissipated-energy density

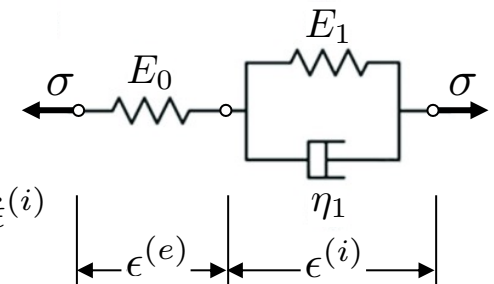
$$Q = \frac{\text{Re}(M)}{\text{Im}(M)}$$



$$\epsilon = \epsilon^{(e)} + \epsilon^{(i)}$$

$$\sigma = E_0 \epsilon^{(e)}$$

$$\sigma = E_1 \epsilon^{(i)} + \eta_1 \dot{\epsilon}^{(i)}$$



Materials with memory

Internal variables and evolution equation

- The memory or path-dependency of a material can be represented through an array of **internal variables** (scalars and second-order tensors)

$$\boldsymbol{\sigma}(\mathbf{X}, t) = \mathbf{f}(\boldsymbol{\epsilon}, T, \boldsymbol{\xi}^t) \equiv \begin{cases} \mathbf{f}(\boldsymbol{\epsilon}, T, \boldsymbol{\xi}) \\ \dot{\boldsymbol{\xi}}_\alpha = g_\alpha(\boldsymbol{\sigma}, T, \boldsymbol{\xi}) \end{cases} \text{ evolution equations}$$

The presence of additional variables in the constitutive laws requires additional constitutive equations, namely **evolution equations**. The hypothesis is that the rate of evolution of the internal variables is also determined from the local state.

- Example: standard solid model

internal variable

$$\xi_1 = \epsilon^{(i)}$$

evolution equation (kinetic equation)

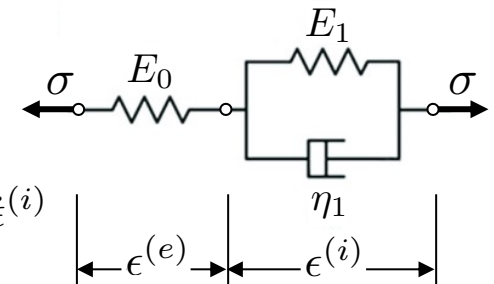
$$\dot{\epsilon}^{(i)} = g_1(\sigma, \xi_1) = \frac{1}{\eta_1} \sigma - \frac{E_1}{\eta_1} \epsilon^{(i)}$$

$$\dot{\epsilon}^{(i)} = g_1(\epsilon, \xi_1) = \frac{E_0}{\eta_1} (\epsilon - \epsilon^{(i)}) - \frac{E_1}{\eta_1} \epsilon^{(i)} \quad (\text{an evolution equation in terms of strain is not always possible})$$

$$\epsilon = \epsilon^{(e)} + \epsilon^{(i)}$$

$$\sigma = E_0 \epsilon^{(e)}$$

$$\sigma = E_1 \epsilon^{(i)} + \eta_1 \dot{\epsilon}^{(i)}$$



Materials with memory

Internal variables and evolution equation

- The memory or path-dependency of a material can be represented through an array of **internal variables** (scalars and second-order tensors)

$$\boldsymbol{\sigma}(\mathbf{X}, t) = \mathbf{f}(\boldsymbol{\epsilon}, T, \boldsymbol{\xi}^t) \equiv \begin{cases} \mathbf{f}(\boldsymbol{\epsilon}, T, \boldsymbol{\xi}) \\ \dot{\boldsymbol{\xi}}_\alpha = g_\alpha(\boldsymbol{\sigma}, T, \boldsymbol{\xi}) \end{cases} \text{ evolution equations}$$

The presence of additional variables in the constitutive laws requires additional constitutive equations, namely **evolution equations**. The hypothesis is that the rate of evolution of the internal variables is also determined from the local state.

Two types ...

- *Physical* internal variables: describe aspects of the local physical-chemical structure which may change spontaneously (e.g., extent of chemical reaction or phase change, density of structural defects).
- *Phenomenological* internal variables: mathematical constructs (e.g., inelastic strain) with a functional dependence with stress (strain) is assumed a priori (i.e., evolution equations).

Materials with memory

Internal variables and thermodynamics

Using conservation of energy, the Clausius-Duhem inequality can be written as

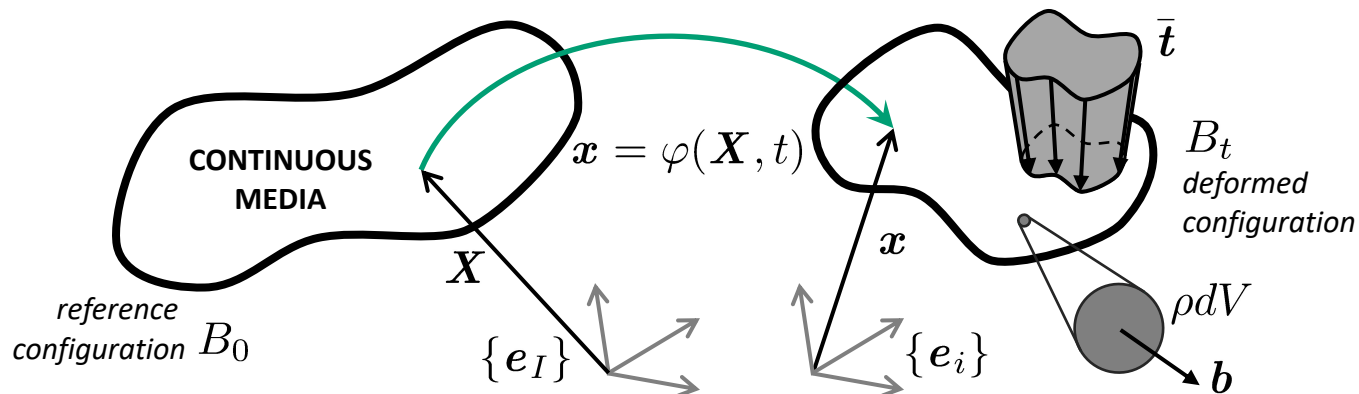
$$\rho T \dot{s}^{\text{int}} = -\rho \left[\frac{1}{\rho_0} \frac{\partial W}{\partial T} + s \right] \dot{T} + \left[\boldsymbol{\sigma} - \frac{\rho}{\rho_0} \frac{\partial W}{\partial \boldsymbol{\epsilon}} \right] : \dot{\boldsymbol{\epsilon}} - \frac{1}{T} \mathbf{q} \cdot \nabla T \geq 0$$

Coleman and Noll made the argument that this inequality must be satisfied for every admissible process.

Let's now consider path-dependent behavior characterized by a set of internal variables and corresponding evolution equations, that is

$$W = \bar{W}(\boldsymbol{\epsilon}, T, \boldsymbol{\xi})$$

$$\dot{\xi}_\alpha = g_\alpha(\boldsymbol{\sigma}, T, \boldsymbol{\xi})$$



Materials with memory

Internal variables and thermodynamics

- Isentropic/Adiabatic processes $\mathbf{q} = \mathbf{0}$, $W(\boldsymbol{\epsilon}, T, \boldsymbol{\xi})$, $\dot{s} \neq 0$ (with $\dot{T} = 0$)

Assuming $\boldsymbol{\epsilon} = \boldsymbol{\epsilon}^{(e)}(\boldsymbol{\sigma}, T) + \boldsymbol{\epsilon}^{(i)}(\boldsymbol{\xi})$, then there exists $W(\boldsymbol{\epsilon}, T, \boldsymbol{\xi})$ if and only if

$$W(\boldsymbol{\epsilon}, T, \boldsymbol{\xi}) = W^{(e)}(\boldsymbol{\epsilon} - \boldsymbol{\epsilon}^{(i)}(\boldsymbol{\xi}), T) + W^{(i)}(\boldsymbol{\xi}, T)$$

$$\dot{W} = \frac{\partial W}{\partial \boldsymbol{\epsilon}} : \dot{\boldsymbol{\epsilon}} + \frac{\partial W}{\partial T} \dot{T} + \sum_{\alpha} \frac{\partial W}{\partial \xi_{\alpha}} \dot{\xi}_{\alpha}$$

DIY

(cont.)

Materials with memory

Internal variables and thermodynamics

- Isentropic/Adiabatic processes $\mathbf{q} = \mathbf{0}$, $W(\boldsymbol{\epsilon}, T, \boldsymbol{\xi})$, $\dot{s} \neq 0$ (with $\dot{T} = 0$)

Assuming $\boldsymbol{\epsilon} = \boldsymbol{\epsilon}^{(e)}(\boldsymbol{\sigma}, T) + \boldsymbol{\epsilon}^{(i)}(\boldsymbol{\xi})$, then there exists $W(\boldsymbol{\epsilon}, T, \boldsymbol{\xi})$
if and only if

$$W(\boldsymbol{\epsilon}, T, \boldsymbol{\xi}) = W^{(e)}(\boldsymbol{\epsilon} - \boldsymbol{\epsilon}^{(i)}(\boldsymbol{\xi}), T) + W^{(i)}(\boldsymbol{\xi}, T)$$

(cont.)

DIY

$$\boldsymbol{\sigma} = \frac{\rho}{\rho_0} \frac{\partial W^{(e)}}{\partial \boldsymbol{\epsilon}^{(e)}}$$

$$\boldsymbol{\sigma} : \dot{\boldsymbol{\epsilon}}^{(i)} - \frac{\rho}{\rho_0} \sum_{\alpha} \frac{\partial W^{(i)}}{\partial \xi_{\alpha}} \dot{\xi}_{\alpha} \geq 0$$

Internal variables and thermodynamics

- Example: standard solid model

DIY

$$W(\epsilon, T, \xi) = W^{(e)}(\epsilon - \epsilon^{(i)}(\xi), T) + W^{(i)}(\xi, T) = \frac{1}{2}E_0(\epsilon - \epsilon^{(i)})^2 + \frac{1}{2}E_1(\epsilon^{(i)})^2$$

Internal variable $\epsilon^{(i)}(\xi) = \xi$

$$\rho = \rho_0 = 1$$

Evolution equation $\dot{\xi} = g(\sigma, \xi) = \frac{\sigma - E_1\xi}{\eta_1}$

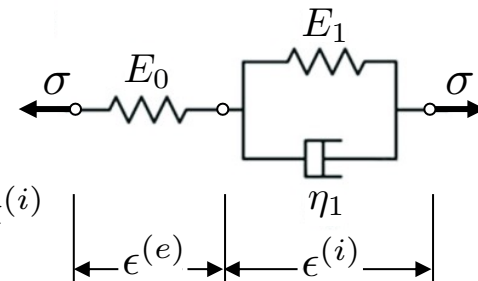
Clausius-Duhem inequality

$$\eta_1(\dot{\epsilon}^{(i)})^2 \geq 0$$

$$\epsilon = \epsilon^{(e)} + \epsilon^{(i)}$$

$$\sigma = E_0\epsilon^{(e)}$$

$$\sigma = E_1\epsilon^{(i)} + \eta_1\dot{\epsilon}^{(i)}$$



Internal variables and thermodynamics

- Example: multiaxial behavior and time integration

DIY

$$W(\boldsymbol{\epsilon}, T, \boldsymbol{\xi}) = W^{(e)}(\boldsymbol{\epsilon} - \boldsymbol{\epsilon}^{(i)}(\boldsymbol{\xi}), T) + W^{(i)}(\boldsymbol{\xi}, T)$$

Internal variable $\boldsymbol{\epsilon}^{(i)}(\boldsymbol{\xi}) = \boldsymbol{\xi}$

$$W^{(i)}(\boldsymbol{\xi}, T) = \frac{1}{2} E_1 \boldsymbol{\epsilon}^{(i)} : \boldsymbol{\epsilon}^{(i)}$$

Evolution equation $\dot{\boldsymbol{\epsilon}}^{(i)} = \frac{\boldsymbol{\sigma} - E_1 \boldsymbol{\epsilon}^{(i)}}{\eta_1}$

Time integration $t_n \rightarrow t_{n+1} = t_n + \Delta t$

- Given $\left\{ \boldsymbol{\epsilon}_{n+1}, \boldsymbol{\sigma}_n, \boldsymbol{\epsilon}_n^{(i)} \right\}$

- Update internal variable $\boldsymbol{\epsilon}_{n+1}^{(i)} = \frac{1}{\eta_1/\Delta t} \boldsymbol{\sigma}_n + \boldsymbol{\epsilon}_n^{(i)} \left[1 - \frac{E_1}{\eta_1/\Delta t} \right]$

- Update stress $\boldsymbol{\sigma}_{n+1} = \frac{\rho_{n+1}}{\rho_0} \frac{\partial W_{n+1}^{(e)}}{\partial \boldsymbol{\epsilon}^{(e)}}$

Lecture 11 – Viscoelastic solids

Any questions?