

ECE 595, Section 10
Numerical Simulations
Lecture 18: FEM for Thermal
Transport

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Outline

- Recap from Monday
- Thermal transfer overview
 - Convection
 - Conduction
 - Radiative transfer

Recap from Monday

- Applications of Beam Propagation Method
 - Tunable Photonic Crystal Fibers
 - Electro-Optic Modulator
 - Electro-Optic Switch

Thermal Transport Mechanisms

- Convection: heat transfer by surface contact with gas or fluid molecules
- Conduction: volumetric heat transfer by propagation of phonons
- Radiative thermal transfer: emission of thermal photons from source to receiver

Thermal Transport: Convection

- Heat transfer by gas or fluid molecules
- Transfer rate per unit area given by:

$$Q = h(T_1 - T_2)$$

- Heat transfer constant h determined by many factors, including material choice, microstructures, fluid flow environment, etc.

Thermal Transport: Conduction

- Volumetric heat transfer through phonon transfer
- Heat transfer rate quantified by Fourier's law:

$$Q = -k\nabla T$$

- Conservation of energy yields:

$$\frac{\partial u}{\partial t} = L - \nabla \cdot Q$$

$$\frac{\partial u}{\partial t} - L = k\nabla^2 T = \frac{k}{\rho c_v} \nabla^2 u \equiv \alpha \nabla^2 u$$

Thermal Transport: Radiative Transfer

- Heat transfer via photon emission
- For a blackbody, total emission follows Stefan-Boltzmann law:

$$P = \sigma T^4$$

- Net thermal transfer between two infinite surfaces becomes:

$$Q = \sigma (T_1^4 - T_2^4)$$

Thermal Transport: Radiative Transfer

- Emission for real materials depends on emissivity
- In thermal equilibrium, Kirchoff's law states emissivity=absorptivity at each wavelength
- Emission spectrum is given by:

$$\frac{dQ}{d\lambda} = \frac{2\pi hc^2 \epsilon(\lambda)}{\lambda^5 [e^{hc/\lambda kT} - 1]}$$

- Blackbody result recovered by setting $\epsilon(\lambda) = 1$ and integrating

Thermal Transport: Modeling

- Convection amounts to a boundary condition in most problems
- Will thus be first combined with conduction
- Strategy:
 - Create FEM grid for thermal convection
 - Impose BC's from convection
 - (Optionally) include radiative transfer from disconnected bodies

Thermal Transport FEM

- Employ Galerkin method to reduce to linear algebra problem as before (see Petr Krysl's step-by-step introduction, Chapter 6):

$$C\dot{T} + (K + H)T = \sum_i L_i$$

- Where:

$$C_{ji} = \int_{S_c} N_j c_V N_i \, dS$$

$$L_{Q,j} = \int_{S_c} N_j Q \, dS$$

$$K_{ij} = \int_{S_c} (\text{grad}N_j) \kappa (\text{grad}N_i)^T \, dS$$

$$L_{q2,j} = - \int_{C_{c,2}} N_j \bar{q}_n \, dC$$

$$H_{ji} = \int_{C_{c,3}} N_j h N_i \, dC$$

$$L_{q3,j} = \int_{C_{c,3}} N_j h T_a \, dC$$

SOFEA: MATLAB FEM Toolbox

- 1D Meshing routine:

```
for j= 1:n+1
    fens=[fens fenode(struct ('id',j,'xyz',[x]));];
    x = x+(L/n);
end
gcells = [];
for j= 1:n
    gcells = [gcells gcell_l2(struct('id',j,'conn',[j j+1]))];
end
```

- Construct finite element block:

```
feb = feblock_defor_taut_wire(struct ('mater',mater_defor,...
    'gcells',gcells,...
    'integration_rule',simpson_1_3_rule,...
    'P',P));
geom = field(struct ('name',['geom'], 'dim', 1, 'fens',fens));
w = 0*clone(geom,'w');
```

SOFEA: MATLAB FEM Toolbox

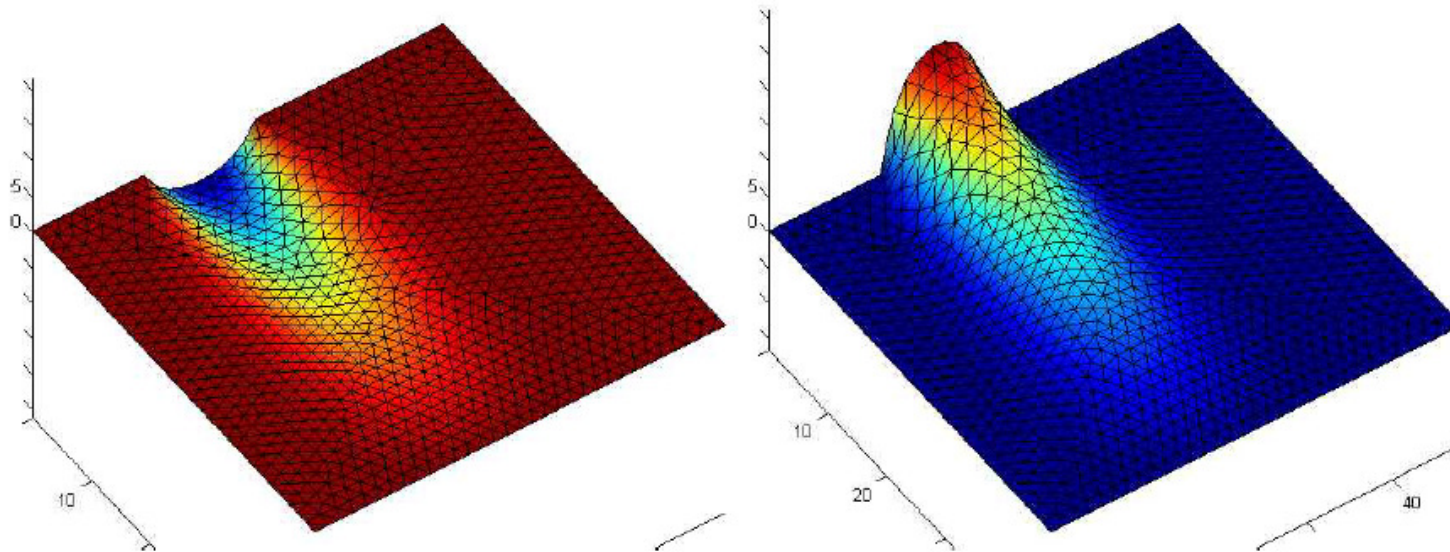
- Apply boundary conditions:

```
fenids=[1]; prescribed=[1]; component=[1]; val=0;
w      = set_etc(w, fenids, prescribed, component, val);
w      = apply_etc (w);
w      = numbereqns (w);
```

- Assemble and solve equations:

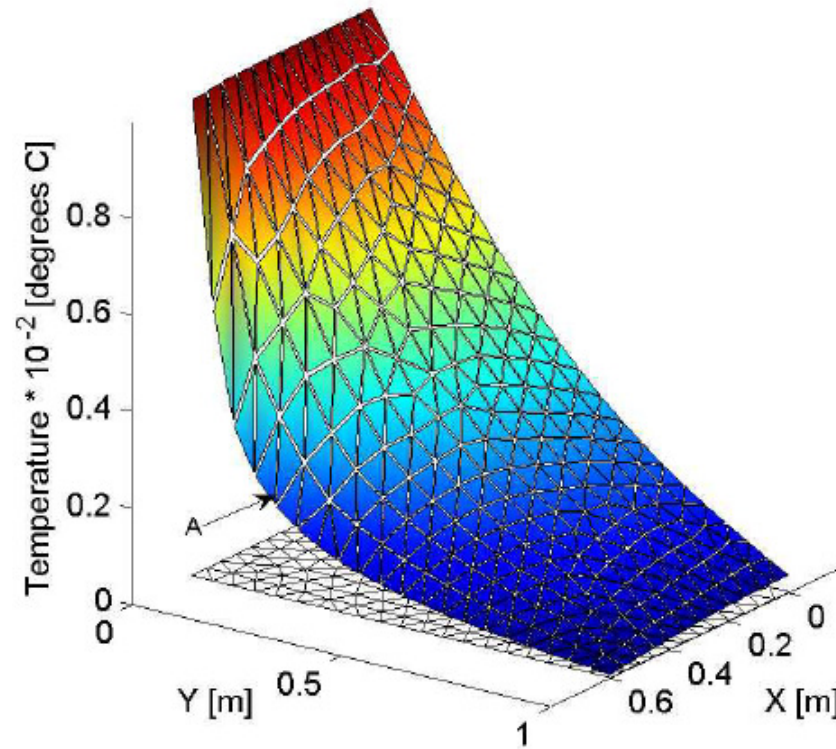
```
K = start (dense_sysmat, get(w, 'neqns'));
K = assemble (K, stiffness(feb, geom, w));
bl = body_load(struct ('magn', inline(num2str(q))));
F = start (sysvec, get(w, 'neqns'));
F = assemble (F, body_loads(feb, geom, w, bl));
w = scatter_sysvec(w, get(K, 'mat')\get(F, 'vec'));
```

Results



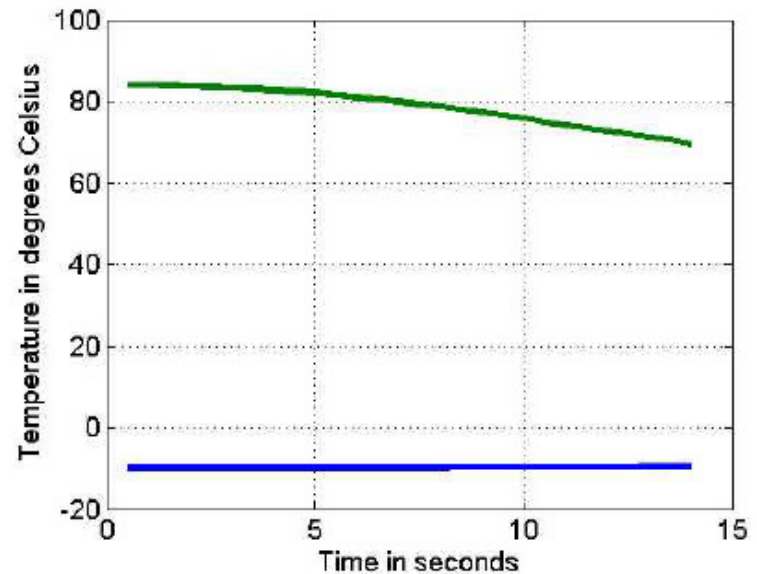
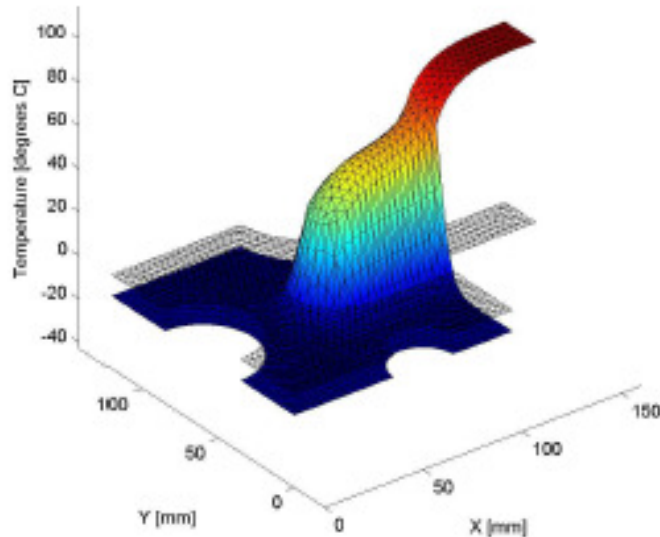
- Steady-state solution for a thermally insulating medium, with a variable temperature placed along one surface

Thermal Conduction: Results



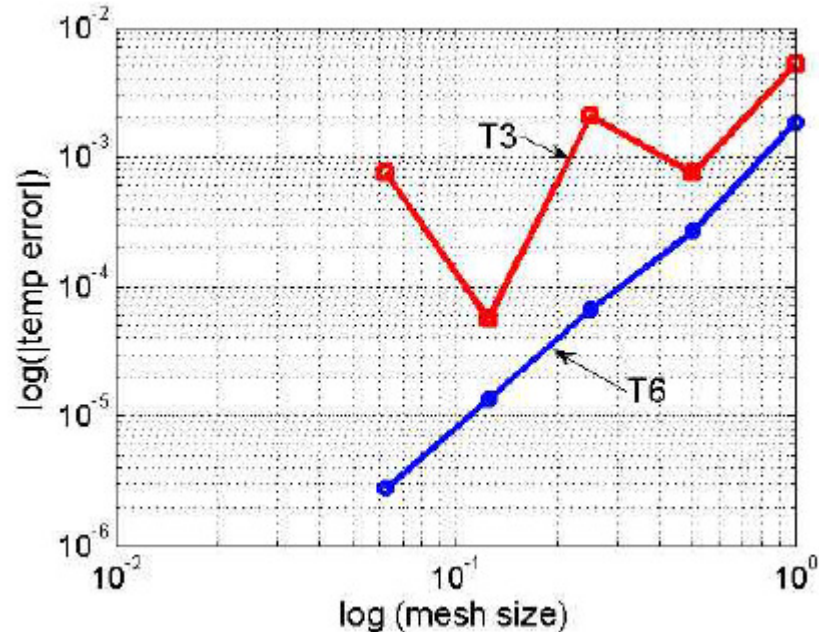
- Steady-state thermal gradient between two adjoining walls with different temperatures

Thermal Conduction: Results



- Transient cooling of a shrink-fitted assembly:
 - In red: highest temperature vs. cooling time
 - In blue: lowest temperature vs. cooling time

Error Evaluation



- Error for linear elements T3 higher overall than quadratic elements T6; both decrease almost quadratically with mesh size

Next Class

- Is on Friday, Feb. 22
- Next time, we will cover other FEM applications in electronic transport