ECE 595, Section 10 Numerical Simulations Lecture 26: Overview of Transfer Matrix Methods

Prof. Peter Bermel March 18, 2013

Recap from Fri., Mar. 8

- Periodic Potential Lab
 - Basic principles
 - Input Interface
 - Exemplary Outputs
- CNTbands
 - Basic principles
 - Input Interface
 - Exemplary Outputs

Outline

- Ray-optics transfer matrix
- Wave-optics matrix methods:
 - T-matrix
 - R-matrix
 - S-matrix

Consider light traveling through an optical element (blue):



- Can capture behavior with 2 rays: ⊥ going in (green); ⊥ going out (red)
- Represent input and output states as ordered pair: (y_k, θ_k)

- Would like to create linear relationship between input and output
- Consider propagation across a distance d:

 $y_2 = y_1 + d\tan\theta_1$

• In paraxial approximation, assume angles are small, such that:

 $\sin \theta \approx \theta$ $\tan \theta \approx \theta$ $\cos \theta \approx 1 - \theta^2/2$

• We can now relate input and output states:

$$y_2 = y_1 + d\theta_1$$
$$\theta_1 = \theta_2$$

• Expressed as a matrix:

$$\begin{pmatrix} y_2 \\ \theta_2 \end{pmatrix} = \begin{pmatrix} 1 & d \\ 0 & 1 \end{pmatrix} \begin{pmatrix} y_1 \\ \theta_1 \end{pmatrix}$$

• In general, can write:

$$\begin{pmatrix} y_2 \\ \theta_2 \end{pmatrix} = \begin{pmatrix} A & B \\ C & D \end{pmatrix} \begin{pmatrix} y_1 \\ \theta_1 \end{pmatrix}$$



• To propagate light through this system:

 $\begin{pmatrix} y_2 \\ \theta_2 \end{pmatrix} = \begin{pmatrix} 1 & d_7 \\ 0 & 1 \end{pmatrix} \begin{pmatrix} 1 & d_6 \\ 0 & 1 \end{pmatrix} \begin{pmatrix} 1 & 0 \\ 0 & \frac{n_4}{n_1} \end{pmatrix} \begin{pmatrix} 1 & d_5 \\ 0 & 1 \end{pmatrix} \begin{pmatrix} \frac{1}{n_1 - n_4} & \frac{0}{n_1} \\ \frac{n_1 - n_4}{Rn_4} & \frac{n_1}{n_4} \end{pmatrix} \begin{pmatrix} 1 & d_4 \\ 0 & 1 \end{pmatrix} \begin{pmatrix} 1 & 0 \\ -1/f & 1 \end{pmatrix} \cdots \begin{pmatrix} y_1 \\ \theta_1 \end{pmatrix}$

http://www.photonics.byu.edu/ABCD_Matrix_tut.phtml

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- If we represent the electric field as two counter-propagating waves: $E(x) = E_+ e^{j\beta x} + E_- e^{-j\beta x}$
- We can use Faraday's law:

$$-\frac{\partial B}{\partial t} = \nabla \times E$$

• To show that:

$$B(x) = \frac{n}{c} \left(E_{-} e^{-j\beta x} - E_{+} e^{j\beta x} \right)$$

• Can calculate each component from total field at *x*=0:

$$E_{+} = \frac{1}{2} \left[E(0) - \frac{c}{n} B(0) \right]$$
$$E_{-} = \frac{1}{2} \left[E(0) + \frac{c}{n} B(0) \right]$$

• Then construct total field at *x*=*L*:

$$E(L) = \frac{1}{2} \left[E(0) - \frac{c}{n} B(0) \right] e^{j\beta L} + \frac{1}{2} \left[E(0) + \frac{c}{n} B(0) \right] e^{-j\beta L}$$

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T-Matrices

• Can represent solutions as T-matrices:

$$\begin{bmatrix} E(L) \\ B(L) \end{bmatrix} = \begin{bmatrix} \cos\beta L & -\frac{c}{n}\sin\beta L \\ -\frac{n}{c}\sin\beta L & \cos\beta L \end{bmatrix} \begin{bmatrix} E(0) \\ B(0) \end{bmatrix}$$

- This approach is known as the transfer matrix
- For multiple layers, can take matrix products

• Special case: quarter-wave stack, where $\beta L = \pi/2$:

$$\begin{bmatrix} E(a) \\ B(a) \end{bmatrix} = \begin{bmatrix} 0 & -\frac{c}{n_2} \\ -\frac{n_2}{c} & 0 \end{bmatrix} \begin{bmatrix} 0 & -\frac{c}{n_1} \\ -\frac{n_1}{c} & 0 \end{bmatrix} \begin{bmatrix} E(0) \\ B(0) \end{bmatrix}$$
$$\begin{bmatrix} E(a) \\ B(a) \end{bmatrix} = \begin{bmatrix} \frac{n_1}{n_2} & 0 \\ 0 & \frac{n_2}{n_1} \end{bmatrix} \begin{bmatrix} E(0) \\ B(0) \end{bmatrix}$$

• Then transmission for M layers is $T = \left(\frac{n_1}{n_2}\right)^{2M}$

T-Matrices

- Clearly, T-matrices see exponentially growing entries
- A major numerical challenge!
- Can reformulate the problem in a more numerically stable fashion:
 - R-matrix method
 - S-matrix method

S- and R-Matrices





Transfer matrix problem between modes propagating up and down

Transfer matrix problem between two polarizations

Two alternative formulations

S-Matrices

- For S-matrix, connect incoming to outgoing fields from
- Mathematically,

$$\begin{bmatrix} u^{(p+1)} \\ d^{(0)} \end{bmatrix} = \begin{bmatrix} T^{(p)}_{uu} & R^{(p)}_{ud} \\ R^{(p)}_{du} & T^{(p)}_{dd} \end{bmatrix} \begin{bmatrix} u^{(0)} \\ d^{(p+1)} \end{bmatrix}$$

• For input from below:

- transmission given by
$$T_{uu}^{(p)}$$

- reflection given by $R_{du}^{(p)}$

R-Matrices

- For R-matrix, connect incoming to outgoing fields from
- Mathematically,

$$\begin{bmatrix} U^{(p+1)} \\ U^{(0)} \end{bmatrix} = \begin{bmatrix} R^{(p)} & R^{(p)} \\ 11 & R^{(p)} \\ R^{(p)} \\ 21 & R^{(p)} \\ 22 \end{bmatrix} \begin{bmatrix} V^{(p+1)} \\ V^{(0)} \end{bmatrix}$$

• U and V can represent E and H fields; then Rmatrix represents field impedance

Next Class

- Is on Wednesday, March 20
- Will continue explaining R- and Smatrices
- Read L. Li, JOSA A 13, 1024-1035