## ECE 695 Numerical Simulations Lecture 20: Transfer Matrices and S<sup>4</sup>

Prof. Peter Bermel March 1, 2017

# Outline

- Periodic solution strategy
  - Stacked periodicity
  - Transverse periodicity
- S-Matrix Simulations
- S4 RCWA solver
  - Capabilities
  - Live demonstration

# S-Matrices

- For S-matrix, connect incoming to outgoing fields from boundaries of region
- Mathematically,

$$\begin{bmatrix} u^{(p+1)} \\ d^{(0)} \end{bmatrix} = \begin{bmatrix} T^{(p)}_{uu} & R^{(p)}_{ud} \\ R^{(p)}_{du} & T^{(p)}_{dd} \end{bmatrix} \begin{bmatrix} u^{(0)} \\ d^{(p+1)} \end{bmatrix}$$

• For input from below:

- transmission from bottom to top given by  $T_{uu}^{(p)}$ - reflection at bottom given by  $R_{du}^{(p)}$ 

## S-Matrices: Periodicity

- What happens if one or more layers are periodic?
- Then there are two types of coupling:
  - Layer-to-layer (refractive)
  - Mode-to-mode (diffractive)
- Can both be treated in a single framework?

#### S-Matrices: Stacked Periodicity

• Recall that:

$$s^{(p)} = \begin{bmatrix} t_{11}^{(p)} - t_{12}^{(p)} t_{22}^{(p)-1} t_{21}^{(p)} & t_{12}^{(p)} t_{22}^{(p)-1} \\ -t_{22}^{(p)-1} t_{21}^{(p)} & t_{22}^{(p)-1} \end{bmatrix}$$

• For quarter wave stack, express in terms of t-matrix elements:  $\tilde{s}^{(p)} = \begin{bmatrix} 1 & 0 \\ 0 & \exp\left(-j\beta \frac{(p)}{m,-}\Delta y_p\right) \end{bmatrix} s^{(p)} \begin{bmatrix} \exp\left(j\beta \frac{(p)}{m,+}\Delta y_p\right) & 0 \\ 0 & 1 \end{bmatrix}$ 

#### S-Matrices: Transverse Periodic Solution

- Divide into layers, uniform in z-direction
- Find Bloch states in each layer
- Calculate transfer function for field amplitudes
- Iteratively develop S-matrix
- Choose inputs from both sides
- Calculate resulting outputs (transmission and reflection) and losses (absorption A=1-T-R)

Whittaker & Culshaw, *Phys. Rev. B* **60**, 2610 (1999) Tikhodeev *et al.*, *Phys. Rev. B* **66**, 045102 (2002)

- Can use a Fourier series expansion in real space of the H-fields:  $\mathbf{H}(\mathbf{r},z) = \sum_{\mathbf{G}} \left( \phi_x(\mathbf{G}) \left[ \hat{\mathbf{x}} - \frac{1}{q} (k_x + G_x) \hat{\mathbf{z}} \right] + \phi_y(\mathbf{G}) \left[ \hat{\mathbf{y}} - \frac{1}{q} (k_y + G_y) \hat{\mathbf{z}} \right] \right) e^{i(\mathbf{k} + \mathbf{G}) \cdot \mathbf{r} + iqz}$
- In momentum space, can represent as:  $h(z) = e^{iqz} \left\{ \phi_x \hat{\mathbf{x}} + \phi_y \hat{\mathbf{y}} - \frac{1}{q} (\hat{k}_x \phi_x + \hat{k}_y \phi_y) \hat{\mathbf{z}} \right\}$
- And then the electric field as:

$$e(z) = \frac{1}{q} e^{iqz} \hat{\eta} \{ [\hat{k}_y \hat{k}_x \phi_x + (q^2 + \hat{k}_y \hat{k}_y) \phi_y] \hat{\mathbf{x}} - [\hat{k}_x \hat{k}_y \phi_y + (q^2 + \hat{k}_x \hat{k}_x) \phi_x] \hat{\mathbf{y}} + q [\hat{k}_y \phi_x - \hat{k}_x \phi_y] \hat{\mathbf{z}} \}$$

• Eigenvalue equation becomes

$$\left[ \begin{pmatrix} \hat{\eta} & 0 \\ 0 & \hat{\eta} \end{pmatrix} \left[ q^2 + \begin{pmatrix} \hat{k}_x \hat{k}_x & \hat{k}_x \hat{k}_y \\ \hat{k}_y \hat{k}_x & \hat{k}_y \hat{k}_y \end{pmatrix} \right] + \begin{pmatrix} \hat{k}_y \hat{\eta} \hat{k}_y & -\hat{k}_y \hat{\eta} \hat{k}_x \\ -\hat{k}_x \hat{\eta} \hat{k}_y & \hat{k}_x \hat{\eta} \hat{k}_x \end{pmatrix} \right] \times \begin{pmatrix} \phi_x \\ \phi_y \end{pmatrix} = \omega^2 \begin{pmatrix} \phi_x \\ \phi_y \end{pmatrix}$$

• More compactly represented as:

 $[\mathcal{H}(q^2 + K) + \mathcal{K}]\phi = \omega^2 \phi$ 

• Where the eigenvectors  $\phi$  have a unique orthonormality condition:

$$\phi_n^T(\omega^2 - \mathcal{K})\phi_{n'} = \delta_{nn'}$$

• Can rephrase:

$$[(\omega^2 - \mathcal{K})\mathcal{E}(\omega^2 - \mathcal{K}) - \omega^2 K]\phi = q^2(\omega^2 - \mathcal{K})\phi$$

• Where *H*-fields are written as:

$$\begin{pmatrix} h_x(z) \\ h_y(z) \end{pmatrix} = \sum_n \begin{pmatrix} \phi_{x_n} \\ \phi_{y_n} \end{pmatrix} (e^{iq_n z} a_n + e^{iq_n(d-z)} b_n)$$

$$h_{\parallel}(z) = \Phi[\hat{f}(z)a + \hat{f}(d-z)b]$$
And where *E*-fields are given by:
$$\begin{pmatrix} -e_y(z) \\ e_x(z) \end{pmatrix} = \sum_n \begin{pmatrix} \hat{\eta} & 0 \\ 0 & \hat{\eta} \end{pmatrix} \left[ q_n^2 + \begin{pmatrix} \hat{k}_x \hat{k}_x & \hat{k}_x \hat{k}_y \\ \hat{k}_y \hat{k}_x & \hat{k}_y \hat{k}_y \end{pmatrix} \right] \times \begin{pmatrix} \phi_{x_n} \\ \phi_{y_n} \end{pmatrix} \frac{1}{q_n} (e^{iq_n z} a_n - e^{iq_n(d-z)} b_n)$$

 $e_{\parallel}(z) = (\omega^2 - \mathcal{K}) \Phi \hat{q}^{-1} [\hat{\mathbf{f}}(z)a - \hat{\mathbf{f}}(d-z)b]$ 

• Interface matrix in WC notation:

$$\begin{pmatrix} \hat{f}_{l}a_{l} \\ b_{l} \end{pmatrix} = I(l,l+1) \begin{pmatrix} a_{l+1} \\ \hat{f}_{l+1}b_{l+1} \end{pmatrix} = \begin{pmatrix} I_{11} & I_{12} \\ I_{21} & I_{22} \end{pmatrix} \begin{pmatrix} a_{l+1} \\ \hat{f}_{l+1}b_{l+1} \end{pmatrix}$$

• Where:  $I(l,l+1) = M_l^{-1}M_{l+1}$ 

$$= \frac{1}{2} \hat{q}_{l} \Phi_{l}^{T} (\omega^{2} - \mathcal{K}_{l+1}) \Phi_{l+1} \hat{q}_{l+1}^{-1} \begin{pmatrix} 1 & -1 \\ -1 & 1 \end{pmatrix} \\ + \frac{1}{2} \Phi_{l}^{T} (\omega^{2} - \mathcal{K}_{l}) \Phi_{l+1} \begin{pmatrix} 1 & 1 \\ 1 & 1 \end{pmatrix}.$$

#### S-Matrix Construction: Recap

• We can relate the *s*-interface matrix to the *t*-interface matrix from before:

$$s^{(p)} = \begin{bmatrix} t_{11}^{(p)} - t_{12}^{(p)} t_{22}^{(p)-1} t_{21}^{(p)} & t_{12}^{(p)} t_{22}^{(p)-1} \\ -t_{22}^{(p)-1} t_{21}^{(p)} & t_{22}^{(p)-1} \end{bmatrix}$$

• Then iteratively construct next S-matrix via:

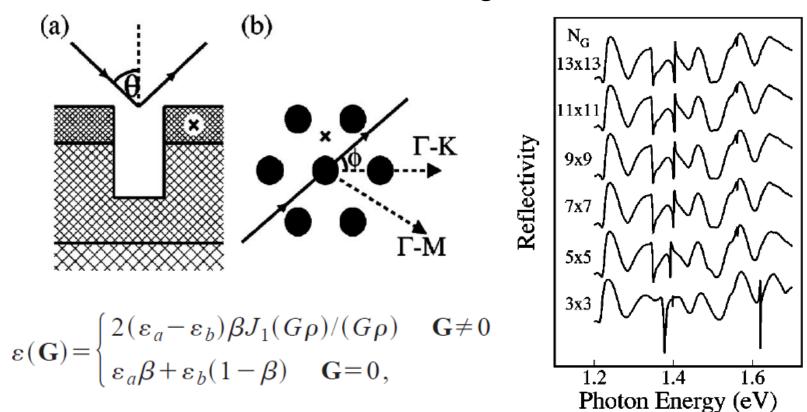
$$\begin{bmatrix} T_{uu}^{(p)} & R_{ud}^{(p)} \\ R_{du}^{(p)} & T_{dd}^{(p)} \end{bmatrix} = \begin{bmatrix} \tilde{t}_{uu}^{(p)} \left[ 1 - R_{ud}^{(p-1)} \tilde{r}_{du}^{(p)} \right]^{-1} T_{uu}^{(p-1)} \\ R_{ud}^{(p-1)} + T_{dd}^{(p-1)} \tilde{r}_{du}^{(p)} \left[ 1 - R_{ud}^{(p-1)} \tilde{r}_{du}^{(p)} \right]^{-1} T_{uu}^{(p-1)} \\ \tilde{r}_{ud}^{(p)} + \tilde{t}_{uu}^{(p)} R_{ud}^{(p-1)} \left[ 1 - \tilde{r}_{du}^{(p)} R_{ud}^{(p-1)} \right]^{-1} \tilde{t}_{dd}^{(p)} \\ T_{dd}^{(p-1)} \left[ 1 - \tilde{r}_{du}^{(p)} R_{ud}^{(p-1)} \right]^{-1} \tilde{t}_{dd}^{(p)} \end{bmatrix}_{\text{ECE 695, Prof. Bermel}}$$

• In WC's notation:

$$\begin{split} S_{11}(l',l+1) &= (I_{11} - \hat{f}_l S_{12}(l',l) I_{21})^{-1} \hat{f}_l S_{11}(l',l) \\ S_{12}(l',l+1) &= (I_{11} - \hat{f}_l S_{12}(l',l) I_{21})^{-1} \\ &\times (\hat{f}_l S_{12}(l',l) I_{22} - I_{12}) \hat{f}_{l+1} \\ S_{21}(l',l+1) &= S_{22}(l',l) I_{21} S_{11}(l',l+1) + S_{21}(l',l) \\ S_{22}(l',l+1) &= S_{22}(l',l) I_{21} S_{12}(l',l+1) + S_{22}(l',l) I_{22} \hat{f}_{l+1} \end{split}$$

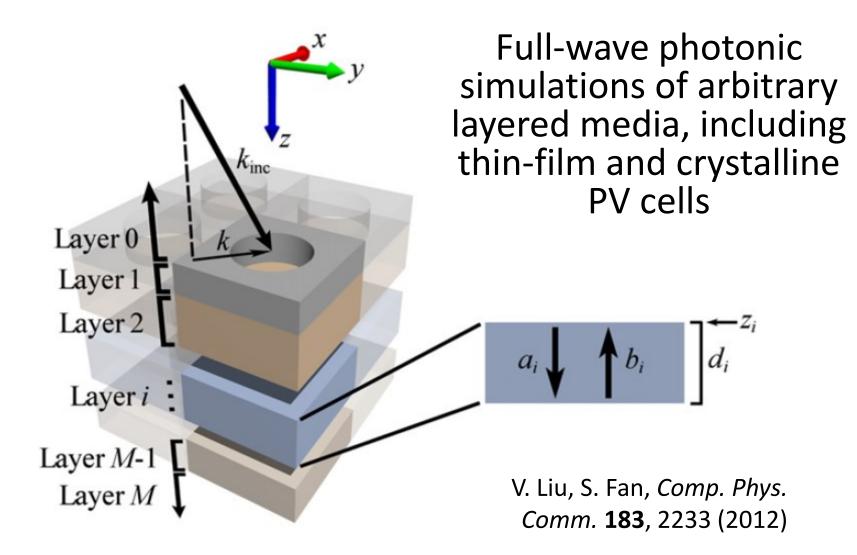
#### **S-Matrix Simulations**

 Transmission through triangular lattice converges as number of plane waves N<sub>G</sub> increases



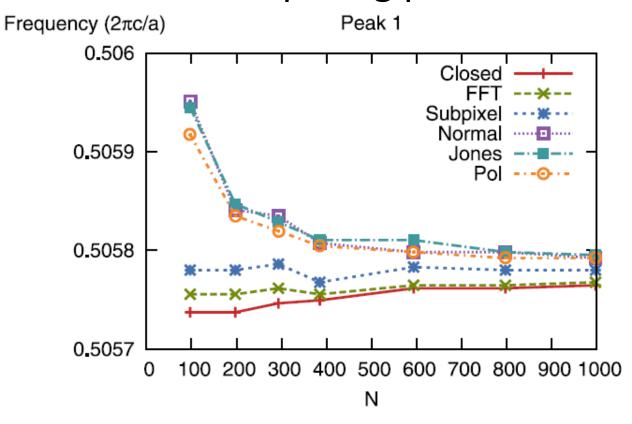
Whittaker & Culshaw, Phys. Rev. B 60, 2610 (1999)

## **Photonic Simulations with S<sup>4</sup>**



# **Photonic Simulations with S<sup>4</sup>**

# Accuracy improves systematically with computing power



V. Liu, S. Fan, Comp. Phys. Comm. 183, 2233 (2012)

ECE 695, Prof. Bermel

# S<sup>4</sup>: Lua Control Files

• Obtain a new, blank simulation object with no solutions:

S = S4. NewSimulation()

• Define all materials:

S:AddMaterial('name', {eps\_real, eps\_imag})

• Add all layers:

S:AddLayer('name', thickness, 'material\_name')

• Add patterning to layers:

S:SetLayerPatternCircle('layer\_name', 'inside\_material', {center\_x, center\_y}, radius)

## S<sup>4</sup>: FMM Formulations

- Specify the excitation mechanism:
- S:SetExcitationPlanewave(

{angle\_phi, angle\_theta}, -- phi in [0,180), theta in [0,360)
{s\_pol\_amp, s\_pol\_phase}, -- phase in degrees
{p\_pol\_amp, p\_pol\_phase})

• Specify the operating frequency:

S:SetFrequency(0.4)

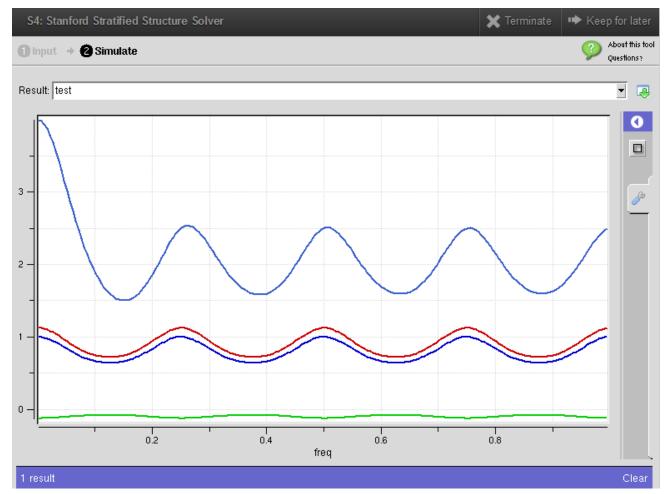
• Obtain desired output:

# S<sup>4</sup>: Input

S4: St	anford Stratified Structure Solver	🗙 Terminate	➡ Keep for later
🛈 Input	+ ② Simulate		About this too Questions ?
Example	transmission_spectrum		•
Input:	New 'N Upload Download		
s s	 binary_grating binary_grating_mpi		
s:	Christ_PRB_70_125_113_2004 Fan_PRB_65_2002 fig2a		
S	fig2b fig3_4 fig6		
s s	fresnel integrate interpolator magneto_halfspace		
S	magneto_slab Ring-Resonator Modes (Cartesian) simple Tikhodeev_PRB_66_45102_2002		
fo	tir transmission_spectrum		
Number	of processors: 1		<b>A</b>
	Walltime: 2h		

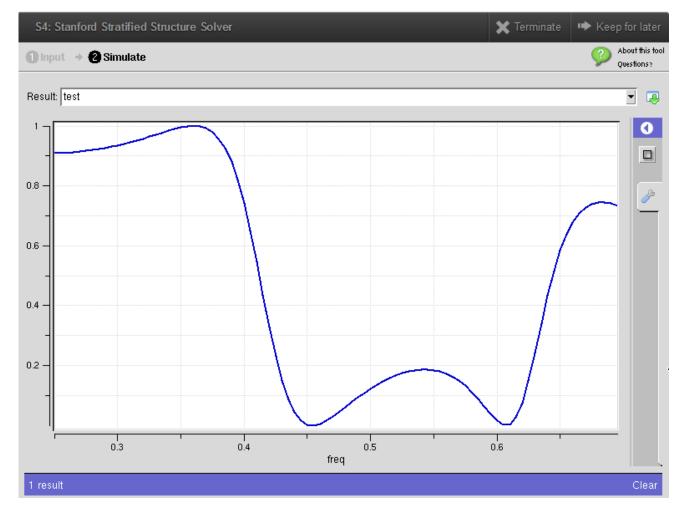
Can choose several examples drawn from the literature

## S<sup>4</sup>: Output



Transmission through multilayer stack matches analytical expression

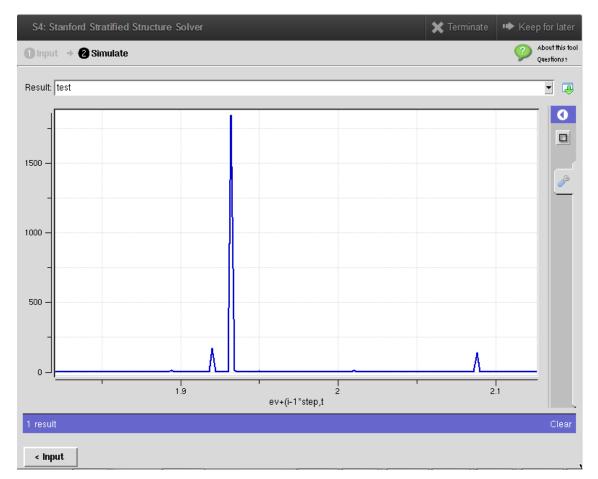
# S<sup>4</sup>: Output



Transmission through 1D square grating of silicon and air

ECE 695, Prof. Bermel

# S<sup>4</sup>: Output



• Transmission from Fig. 4 of Tikhodeev *et al., Phys. Rev. B* 66, 045102 (2002).

#### S-Matrix Method: Advantages

- No *ad hoc* assumptions regarding structures
- Applicable to wide variety of problems
- Suitable for eigenmodes or high-Q resonant modes at single frequency
- Can treat layers with large difference in length scales
- Computationally tractable enough on single core machines

## S-Matrix Method: Disadvantages

- Accurate solutions obtained more slowly as the following increase:
  - Number of layers
  - Absolute magnitude of Fourier components (especially for metals)
  - Number of plane-wave components (~N<sup>3</sup>)
- Relatively slow for broad-band problems (time-domain is a good alternative)

# Next Class

- Is Friday, Mar. 3
- Next time, we will continue with transfer matrix models, focusing on CAMFR