## SCS Unit Hydrograph

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## SCS Dimensionless Unit Hydrograph



Figure 9. Dimensionless unit hydrograph.
"Victor Mockus worked out the NRCS unit hydrograph methodology based upon many natural unit hydrographs from small watersheds in widely varying locations. NRCS has taken an average unit hydrograph from many small agricultural watersheds in the Midwest and has made it dimensionless" - USDA Module 107, Hydrograph Development

Ratios for dimensionless unit hydrograph and mass curve.

| Time <br> Ratios <br> $\left(\mathrm{t} / \mathrm{t}_{\mathrm{p}}\right)$ | Discharge <br> Ratios <br> $\left(\mathrm{q} / \mathrm{q}_{\mathrm{p}}\right)$ | Mass Curve <br> Ratios <br> $\left(\mathrm{Q}_{\mathrm{a}} / \mathrm{Q}\right)$ |
| :--- | :--- | :--- |
| 0.0 | 0.000 | 0.000 |
| 0.1 | 0.030 | 0.001 |
| 0.2 | 0.100 | 0.006 |
| 0.3 | 0.190 | 0.012 |
| 0.4 | 0.310 | 0.035 |
| 0.5 | 0.470 | 0.065 |
| 0.6 | 0.660 | 0.107 |
| 0.7 | 0.820 | 0.163 |
| 0.8 | 0.930 | 0.228 |
| 0.9 | 0.990 | 0.300 |
| 1.0 | 1.000 | 0.375 |
| 1.1 | 0.990 | 0.450 |
| 1.2 | 0.930 | 0.522 |
| 1.3 | 0.860 | 0.589 |
| 1.4 | 0.780 | 0.650 |
| 1.5 | 0.680 | 0.700 |
|  |  |  |


| Time <br> Ratios <br> $\left(\mathrm{t} / \mathrm{t}_{\mathrm{p}}\right)$ | Discharge <br> Ratios <br> $\left(\mathrm{q} / \mathrm{q}_{\mathrm{p}}\right)$ | Mass Curve <br> Ratios <br> $\left(\mathrm{Q}_{\mathrm{a}} / \mathrm{Q}\right)$ |
| :--- | :--- | :--- |
| 1.6 | 0.560 | 0.751 |
| 1.7 | 0.460 | 0.790 |
| 1.8 | 0.390 | 0.822 |
| 1.9 | 0.330 | 0.849 |
| 2.0 | 0.280 | 0.871 |
| 2.2 | 0.207 | 0.908 |
| 2.4 | 0.147 | 0.934 |
| 2.6 | 0.107 | 0.953 |
| 2.8 | 0.077 | 0.967 |
| 3.0 | 0.055 | 0.977 |
| 3.2 | 0.040 | 0.984 |
| 3.4 | 0.029 | 0.989 |
| 3.6 | 0.021 | 0.993 |
| 3.8 | 0.015 | 0.995 |
| 4.0 | 0.011 | 0.997 |
| 4.5 | 0.005 | 0.999 |
| 5.0 | 0.000 | 1.000 |

Figure 16A-1 Dimensionless curvilinear unit hydrograph and equivalent triangular hydrograph


Source: USDA NRCS Part 630 Hydrology National Engineering Handbook

## Finding Qp for SCS Triangular UH

For UH, the area of triangle = unit depth of water

$\mathrm{T}_{\mathrm{p}}$


$$
\frac{1}{2}\left(2.67 T_{p}\right)\left(Q_{p}\right)=1 \text { inch }
$$

For US units, $Q p$ is in cfs, $T p$ is in hours and the depth is in inch. The depth is converted to volume by multiplying it with Area in square miles

$$
\frac{1}{2}\left(2.67 T_{p} * 60 * 60\right)\left(Q_{p}\right)=\left(\frac{1}{12}\right) * \mathrm{~A}(5280 * 5280)
$$

After simplifying the above expression, you get the following

$$
Q_{p}=\frac{483.4 * A}{T_{p}}
$$

If you do the same analysis using SI units, you get the SI version of Qp.

## $\mathrm{Q}_{\mathrm{p}}$ for US and SI Units

When watershed area (A) is in square miles, $Q p$ is in cfs using the following expression. Tp is in hours

$$
Q_{p}=\frac{483.4 * A}{T_{p}}
$$

When watershed area (A) is in square kilometers, $Q p$ is in $\mathrm{m} 3 / \mathrm{s}$ using the following expression. Tp is in hours

$$
Q_{p}=\frac{2.08 * A}{T_{p}}
$$

## Finding Tp

$T_{p}$ is time to discharge peak, which is also equal to rainfall duration/2 plus the lag time as shown in the figure below. $\mathrm{T}_{\mathrm{c}}$ is time of concentration


$$
\begin{gathered}
\mathrm{T}_{\mathrm{p}}=\frac{t_{R}}{2}+t_{l a g} \\
t_{\text {lag }}=0.6 \mathrm{~T}_{\mathrm{c}}
\end{gathered}
$$

## Expression for $\mathrm{T}_{\mathrm{c}}$

$$
T_{c}=\frac{l^{0.8}(S+1)^{0.7}}{1140 Y^{0.5}}
$$

- $\mathrm{T}_{\mathrm{c}}$ is time of concentration(hr)
- $\ell$ is maximum flow length (ft)
- $Y$ is average watershed slope (\%)
- S is maximum potential retention (inch)
- $S=(1000 / C N)-10$
- CN is curve number

