Deformation of the North American Plate Interior from a Decade of Continuous GPS Measurements

E. Calais
Purdue University, Department of Earth and Atmospheric Sciences, West Lafayette, Indiana, USA

J.Y. Han
Purdue University, Department of Geomatics, West Lafayette, Indiana, USA

C. DeMets
University of Wisconsin, Department of Geology and Geophysics, Madison, Wisconsin, USA

J.M. Nocquet
CNRS, UMR6526 Géosciences Azur, Valbonne, France

Abstract. A combination of two independent geodetic solutions using data from close to 300 continuous GPS stations covering the central and eastern U.S. shows that surface deformation in the North American plate interior is best fit by a model that includes rigid rotation of North America with respect to ITRF2000 and a component of strain qualitatively consistent with that expected from Glacial Isostatic Adjustment (GIA). After correcting for the North American plate motion, residual horizontal velocities show a north-to-south deformation gradient of ∼1 mm yr$^{-1}$, mostly localized between 1000 and 2200 km from the GIA center, corresponding to strain rates of about 10$^{-9}$ yr$^{-1}$. At distances farther than 2100 km from the GIA center, horizontal residual velocities are random with no evidence for regions of elevated strain rates. In particular, we find no detectable residual motion at the 95% confidence level in the New Madrid Seismic Zone, where the average weighted misfit of 0.7 mm yr$^{-1}$ is the same as the weighted misfit of our rigid plate model. Vertical velocities show (1) a maximum uplift rate of 10 mm yr$^{-1}$ at the assumed GIA center, (2) a hinge line located 1500 km from that center, and (3) a subsidence rate up to 1.4 mm yr$^{-1}$ in the forebulge, with a maximum located about 2000 km from the GIA center. Our results have the potential to better constrain Glacial Isostatic Adjustment models and contribute to a better definition of stable North America for tectonic and geodetic applications.

1. Background

Large earthquakes within stable plate interiors are direct evidence that significant amounts of elastic strain can accumulate along geologic structures far from plate boundary faults, where the vast majority of seismic energy is released. The 1811-1812 New Madrid events in the Mississippi valley are classical examples of large intraplate earthquakes (e.g., Nuttli, 1983; Johnston, 1996; Hough et al., 2006; Figure 1), as is the 1905-1957 sequence of four M8 and greater earthquakes in Mongolia (Baljinnyam et al., 1993). Because significant intraplate earthquakes are infrequent and strain rates in continental interiors are so low, neither the rates and pattern of intraplate strain are well constrained, nor are the mechanism(s) responsible for strain accumulation and release on faults inside plates.

Based on the scatter of GPS station velocities with respect to the predictions of best-fitting angular velocity vectors, prior geodetic studies have established an approximate upper bound of 2 mm yr$^{-1}$ for residual motions across the Central and Eastern U.S. (e.g., Argus and Gordon, 1996; Dixon et al., 1996; Newman et al., 1999; Kogan et al., 2000; Sella et al., 2002; Marquez-Azua and DeMets, 2003). Gan and Prescott (2001) additionally reported evidence for elevated strain in the south central United States. Though slow by the standards of most plate boundary zones, deformation of 2 mm yr$^{-1}$ nonetheless implies significant seismic hazard over a period of centuries to millennia if it represents elastic strain that accumulates over a several hundred kilometer-wide zone such as the New Madrid seismic zone. Practical considerations thus motivate efforts, including our own, to better quantify local-, regional-, and possibly plate-scale strain from the North American plate GPS velocity field.

Deglaciation of the continental interior following the last ice age has also affected the present velocity field through the still incomplete viscoelastic response of the mantle to the removal of the Laurentide ice sheet that covered Canada and parts of the northern United States until ∼20,000 years ago (e.g., Peltier, 1986; Davis and Mitrovica, 1996). The predicted horizontal surface responses to ice unloading for a range of assumed mantle viscosity structures and likely spatial and temporal scenarios for deglaciation vary from no faster than 1 mm yr$^{-1}$ (e.g., the ICE-3G/VM1 model of Peltier (1994)) to as fast as ∼2 mm yr$^{-1}$ (e.g., the ICE-4G/VM2 model Peltier (1996)) integrated between the Great Lakes and the Gulf of Mexico. Modern space geodetic measurements in North America support the predicted existence of significant glacial isostatic adjustment (GIA), particularly in the vertical. Argus et al. (1999) demonstrate that very long baseline interferometry and satellite laser ranging measurements are better fit by the VM1 model than VM2, despite the few such measurements (fewer than 10) that were then available. More recently Park et al. (2002) compare GIA model predictions to vertical velocities from 60 continuous GPS stations in the northeastern...
U.S. to estimate best-fit viscosities of $2 \times 10^{20}$ Pa.s and 4.1 to 5.4 $\times 10^{21}$ Pa.s for the upper and lower mantle, respectively. Independent of the lithospheric thickness. Both horizontal and vertical GPS velocities can thus be used to constrain GIA model parameters in North America.

Finally, the existence of a link between GIA and intraplate earthquakes in North America has been hypothesized (e.g., Stein et al., 1979; Hasegawa and Basham, 1989). Balz and Zoback (2001) proposed that the melting of the Laurentide ice sheet has resulted in increased seismicity in the New Madrid area in the Holocene. Wu and Johnston (2000), however, find that GIA may significantly contribute to seismicity down to the Wabash Valley Seismic Zone in northern Indiana, but not in the more distant New Madrid Seismic Zone. More recently, Mazzotti et al. (2005) compared local GPS results in the St Lawrence valley, Québec, with seismic catalog statistics and GIA models and proposed that most of the deformation related to GIA is released by large earthquakes in the Charlevoix Seismic Zone (Québec). Plate-wide GPS measurements in North America therefore have the potential to contribute to a better understanding of a possible link between GIA and seismic hazard.

We present a new assessment of intraplate deformation in the North American plate interior based on data from more than 300 continuous GPS stations covering the central and eastern U.S. and Canada, spanning the 1993-2005 period. Our two principal objectives are to quantify deformation associated with glacial isostatic adjustment (GIA) caused by ice unloading of large areas of Canada and the northern United States at the end of the Wisconsin Ice Age, and regional strain associated with the New Madrid Seismic Zone. We exploit the full, plate-scale GPS velocity field to estimate rigorous upper bounds on assumed plate-scale deformation in a manner fundamentally different than prior studies, which use the weighted root-mean-square misfit to their GPS velocities to estimate an upper bound on plate non-rigidity.

The technical aspects of our work include three key elements: (1) the comparison and combination of independent geodetic solutions, (2) the use of as many continuous stations as possible, and (3) the use of several independent techniques for seeking significant local- to plate-scale departures from a simple rotating-plate model. An important unresolved issue in determining realistic uncertainties for GPS site velocities is the degree to which non-tectonic factors, such as site-specific (e.g., ground contraction related to excavation), gravity-driven downslope movement, or temperature-induced monument deformation (GIA) caused by ice unloading of large areas of Canada and the northern United States at the end of the Wisconsin Ice Age, and regional strain associated with the New Madrid Seismic Zone. We exploit the full, plate-scale GPS velocity field to estimate rigorous upper bounds on assumed plate-scale deformation in a manner fundamentally different than prior studies, which use the weighted root-mean-square misfit to their GPS velocities to estimate an upper bound on plate non-rigidity.

2. GPS Data and Processing

2.1. GPS Data

The GPS data we use are principally from the Continuously Operating Reference Station network (CORS) coordinated by the National Geodetic Survey (NGS) (Snay et al., 2002; http://www.ngs.noaa.gov/CORS/) (Figure 2). We also use data from sites that have been contributing to the International GPS Service for Geodynamics (IGS) since 1992 (in particular continuous sites in Canada operated by the Geodetic Survey Division of Natural Resources Canada) and data from the GAMA network (operated by the Center for Earthquake Research and Information, University of Memphis) that covers the New Madrid seismic zone. Numerous monument types, many of unknown stability, are employed at CORS sites, reflecting the varying requirements of the broad CORS user community. IGS site monuments are designed for precise geodetic applications and are presumably more stable. Most GAMA sites use 60' steel H-beams (10" flange, 10" web) driven to refusal into the ground, except for sites MACC and CJTR, installed on the western edge of the Mississippi embayment, that use 6-9"x4"-diameter steel pipes cemented into bedrock.

Although a total of 484 sites are (or have been) operating in the study area (Figure 2), only 286 have an observation time span longer than 3 years, the minimum necessary to average out the effects of unmodeled seasonal processes such as hydrological, atmospheric loading, or tropospheric heterogeneities (Blewitt and Lavallée, 2002). For this study, although we processed all available continuous GPS sites in the central and eastern U.S. and Canada, we only use sites with at least 3 years of continuous observations. Figure 3 illustrates the distribution of GPS sites in stable North America. The bulk of the sites have been operating for less than 4 years, with a sharp increase in the number of sites 3.5 years ago. This also means that in 3 years the number of CGPS sites usable for tectonic studies will have increased by about a third. As several states are currently densifying their GPS infrastructure for commercial applications, these numbers will rise even more in the near future.

2.2. Data Processing

We have processed up to 12 years of continuous data at about 450 continuous GPS sites in the central and eastern U.S. and Canada. Daily data since Jan. 1, 1993 have been processed at the University of Wisconsin using the GIPSY-OASIS software (Zumberge et al., 1997) and data since Jan. 1, 1994 have been processed at Purdue University using the GAMIT-GLOBK software (King and Bock, 2001). The GIPSY and GAMIT processing procedures we employ differ significantly and are described below.

2.2.1. GIPSY-OASIS processing

The GIPSY-OASIS solution is based on the precise point positioning analysis strategy described by Zumberge et al. (1997). It uses free-network satellite orbits and satellite clock offsets obtained from the NASA Jet Propulsion Laboratory (JPL). Site coordinates determined from the analysis of the GPS phase and pseudo-range observables are initially defined in a fiducial-free reference frame and subsequently transformed into the International Terrestrial Reference Frame 2000 (ITRF2000; Altamimi et al., 2002) using 7-parameter Helmert transformations that align the daily coordinates of a selected subset of ITRF2000 fiducial sites with the fiducial-free coordinates of the same subset of sites. No attempt was made to resolve integer phase ambiguities.

Although the covariances for each site’s daily Cartesian coordinates were calculated and propagated into estimates of each site’s velocity (described below), all inter-site coordinate covariances are implicitly assigned values of
zero, a known shortcoming of the precise point positioning technique. For a similar point-positioned GIPSY solution, Marquez-Azua and DeMets (2003) demonstrate the existence of strong correlations and hence non-zero covariances between the daily coordinates of GPS stations out to interstation separations of several thousand kilometers, contrary to the assumption of zero interstation noise. They describe a time- and distance-weighted stacking algorithm that effectively estimates and removes this common-mode daily and longer-period noise, thereby reducing the interstation coordinate covariances to values close to zero. We apply the same common-mode error estimation correction to the present GIPSY solution.

Station velocities are calculated by a linear fit to the uncorrected position time series, including estimation of antenna phase center offsets where such offsets are not specified in station site logs. Following estimation of all site velocities relative to ITRF2000, residuals for each time series are gathered and used to estimate and minimize inter-station correlated noise, after which the corrected daily station positions are again regressed to estimate a refined station velocity. Typical white noise magnitudes in the north and east components are 1.5-2 mm and 3-3.5 mm, respectively. Larger noise in the east component is a likely consequence of unresolved integer phase ambiguities. Station velocity uncertainties are estimated using the Mao et al. (1999) uncertainty estimation algorithm, site-specific estimates of white and flicker noise, and an assumed 1 mm yr^{-0.5} of random monument walk. Prior to its combination with other velocity solutions described below, the GIPSY velocity solution is converted into a Solution Independent EXchange (SINEX) file that contains the estimated station positions and velocities and their covariance matrix for the entire time period considered (1993.0-2005+).

2.2.2. GAMIT-GLOBK processing

The GAMIT-GLOBK solution uses double-differenced GPS phase measurements to estimate daily station coordinates, satellite state vectors, 7 tropospheric delay parameters per site and day, horizontal tropospheric gradients, and phase ambiguities using IGS final orbits and earth orientation parameters. We apply elevation-dependent antenna phase center models following the tables recommended by the IGS, solid Earth and polar tide corrections following the IERS standards (IERS, 1996), and ocean loading corrections using the CSR1.0 ocean tide model (Eanes and Schuh, 1999) with the 8 principal diurnal and semidiurnal tidal constituents. For processing time considerations, we divided the network into regional subnetworks of about 25 sites each. All subnetworks share 6 common IGS sites (AOML, USNO, ALGO, NLID, MDO1, AMCC) determined in ITRF2000. These sites serve to tie the subnetworks together and with the ITRF. We then produce position time series that we use to estimate site-specific parameters for a noise model that includes white and random-walk processes. We finally combine the (unconstrained) daily solutions for each subnetwork into a single, unconstrained, position-velocity solution while accounting for site-specific noise parameters. That final solution is then converted into a SINEX file that contains the estimated station positions and velocities and their complete covariance matrix for the entire time period considered (1994.0-2005+).

2.2.3. Other solutions used

In addition to the GAMIT and GIPSY solutions described above, we use the global solutions provided by the IGS, which results from the combination of individual solutions from IGS analysis centers, goes back to February 1999, and include a few sites in the central and eastern US. Finally, we use the full definition (i.e., estimates and complete covariance matrix) of the ITRF2000 (Altamimi et al., 2002). The ITRF2000 is the current realization of the International Terrestrial Reference System (ITRS) published by the International Earth Rotation Service (IERS). Using the ITRF2000 in the combination of permanent GPS solutions ensures the consistency of the resulting solutions at a continental scale. For instance, Altamimi et al. (2002) show that global-scale GPS solutions are not consistent among themselves in the definition of the scale factor and the center of mass of the Earth. This may have a significant impact on continental-scale GPS-derived velocities, in particular for the vertical component. The ITRF2000, on the other hand, includes 3 VLBI and 7 SLR solutions in order to ensure the best definition of the scale factor and the Earth’s center of mass, as well as their time derivatives. Consequently, using the ITRF2000 solution as a backbone for the combination of individual GPS solutions ensures the origin and scale stability of our combined solution. Finally, the ITRF2000 includes a NOAA solution for the CORS GPS network, with data until 2000.

2.3. Combination Procedure

A key aspect of our work is the geodetic combination of independent geodetic site coordinate and velocity solutions. Rigorous combination of alternative geodetic solutions offers a number of important advantages over using a single velocity solution, including averaging down of random and any systematic errors associated with individual processing strategies and cross-checking of the independent solutions, definition of a single consistent reference frame for the combined solutions, and realistic estimates of the uncertainty. We use the combination algorithm developed by Altamimi et al. (2002), also used to calculate ITRF2000, starting with minimally constrained geodetic solutions. The combination consists of simultaneously estimating, for each site i in solution s (s = GAMIT, GIPSY, IGS, ITRF2000), the velocity \( \dot{X}_{i,\text{comb}} \) and a 14-parameter transformation between the individual and the combined solution using:

\[
\dot{X}_i = \dot{X}_{i,\text{comb}} + (t_s - t_0)\dot{X}_i^{\text{comb}} + T_0 + D_0 \dot{X}_{i,\text{comb}} + R_0 X_{i,\text{comb}}^0 + \dot{X}_i^{\text{comb}}
\]

(1)

\[
\dot{X}_i = \dot{X}_{i,\text{comb}} + T_0 + D_0 \dot{X}_{i,\text{comb}} + R_0 X_{i,\text{comb}}^0
\]

(2)

where \( \dot{X}_i^{\text{comb}} \) is the position of site \( i \) in solution \( s \) at epoch \( t_s \), \( \dot{X}_{i,\text{comb}}^0 \) the estimated position of site \( i \) at epoch \( t_0 \), and \( X_{i,\text{comb}}^0 \) its final velocity in the combination, \( T_0, D_0, R_0 \) and \( \dot{X}_i^{\text{comb}} \) are the transformation parameters between individual solutions \( s \) and the combined solution and their time derivatives, \( t_s \) is the epoch of minimal position variance for the solution \( s \), which is generally the middle point of the observation time span included in the solution, and \( t_0 \) is the epoch of expression of the transformation parameters.

The reference frame definition in the combination is implemented by imposing the 14-parameter transformation between ITRF2000 and the combined solution to be zero (no translation, scale factor, or rotation and no rate of change of these parameters). The resulting velocity field is therefore expressed in ITRF2000.

From the preliminary combination, an a posteriori variance factor \( \sigma_s^2 \) is estimated for each individual solution \( s \) in the inversion, at the same time as the other parameters. This variance factor is then applied to the covariance matrix of the corresponding individual solution in an iterative way until both individual \( \sigma_s^2 \) and the global a posteriori variance factor equal unity. As a result of this iterative scaling, formal errors of the combined solution depend on the variance of the individual solutions before the combination, but also
on the level of agreement between solutions in the combina-
tion.

2.4. Statistics of the Combination

The result of the combination is a SINEX file in which positions and velocities are expressed in ITRF2000. We ob-
tain variance scaling factors ranging from 0.7 to 12.2 (Ta-
ble 1), consistent with empirical scaling factors derived from
time series analysis (Zhang et al., 1997, Mao et al., 1999,
Williams, 2003). The GIPSY solution has a lower variance
factor because velocity uncertainties were estimated with a
model that includes white, flicker, and random walk noise.
The level of agreement between solutions and the combina-
gion, given by the weighted RMS (WRMS) shown in Table 1,
is on the order of 0.5 mm yr\(^{-1}\) or better for the horizon-
tal components.

Two of the solutions included in the combination (GAMIT and GIPSY solutions) account for colored noise in
the velocity error estimates. In addition, the iterative vari-
ance scaling scheme used here results in velocity uncertain-
ties in the combination that are larger than in the individ-
ual solutions (except for the GIPSY solution, as mentioned
above). The final uncertainties of the combined solution
tend to be somewhat conservative.

Figure 4 shows that velocity uncertainties decrease
rapidly during the first 2.5 to 3 years of continuous mea-
surements, consistent with predictions by Blewitt and Lavallée
(2002). Velocity uncertainties decrease more slowly there-
after, reflecting the longer periods that are required to av-
crage down the flicker and random walk noise that affects
GPS monument motions. The best determined site veloc-
ties (~11 years of continuous data) have respective hori-
zontal and vertical standard deviations of about ±0.2 mm yr\(^{-1}\)
and ±0.6 mm yr\(^{-1}\).

One useful outcome of our analysis is a comparison of the
individual GAMIT and GIPSY solutions for a large
number of sites and over a long time period. Applying
procedures outlined in the preceding subsection, we esti-

mated and applied a 14-parameter Helmert transforma-
tion between the individual GIPSY and GAMIT solutions and
the IGS combined solution using 28 common IGS sites.
We then subtracted velocities predicted by the best-fitting
North America-ITRF2000 angular velocity vector described
below from the resulting GAMIT and GIPSY velocity fields
and compared residual velocities at the sites common to
the two solutions (Figure 5). We find that the horizontal com-
ponents of the GAMIT and GIPSY velocities agree within
0.6 mm yr\(^{-1}\) on average, with a negligible bias (0.3 and
-0.1 mm yr\(^{-1}\) for the EW and NS components, respectively).
Differences in the vertical component are larger, typically
within 3 mm yr\(^{-1}\) of their mean value.

3. Analysis of the velocity field

The resulting velocity field describes surface motions with
respect to ITRF2000 (Figure 6A), illustrating the well-
known counter clockwise rotation of the North American
plate in a no-net-rotation frame. We next use the new ve-
locity field to define North American plate motion and use
residual velocities with respect to the new best-fitting refer-
ence frame to describe areas of the plate where significant
deformation appears to be occurring.

3.1. Defining rigid North America

Efforts to detect and model strain anomalies in the
North American plate interior that are caused by tectonic
processes, glacial isostatic adjustment (GIA), or possibly
groundwater withdrawal require a well-determined plate ref-
ence frame. A purely kinematic end-member approach for
defining such a frame is to exclude a priori all sites in geo-
graphic areas where deformation could occur. Alternatively,
one can assimilate the entire GPS velocity field into defor-
mation models while solving for the rotation, translation,
and possibly scale factor that define the frame (e.g., Ble-
witt et al., 2005). The former approach avoids the need
for modeling assumptions beyond that of the rigid plate as-
sumption, but decreases the number and geographic expanse
of sites that are used to define the frame and thus reduces
the potential accuracy and precision of the plate angular
velocity vector. The latter approach makes use of the full
spatial coverage of the velocity field, but introduces model-
ing tradeoffs between the plate angular velocity vector and
the parameters used to describe the a priori physical model.

For the analysis below, we use the former, purely kine-
matic, approach. We use only the velocities of GPS sites
located east of 110°W, thereby avoiding potential contam-
ination of the velocity field by possible slow deformation
west of the Rio Grande rift and central Colorado. For sites
east of 110°W, we treat the area where the plate interior
is potentially affected by distributed deformation as an un-
known and use the F-statistic introduced by Stein and Gor-
don (1984) to identify the approximate geographic limits
of areas affected by GIA. Although the Stein and Gordon
(1984) F-test is designed to detect narrow or wide plate
boundaries between rigid, independently moving plates, it
can also be applied to detection of GIA at sites in southern
Canada and the northern U.S., where the GIA response
is generally to the south and is sufficiently uniform in magni-
tude (±1 mm yr\(^{-1}\)) such that it can be well approximated
by a slow counterclockwise rotation about a pole that is suit-
ably located to predict southward motion in Canada. The
net velocity field of sites in areas affected by GIA is thus well
approximated by a single angular velocity vector that is the
sum of the North American plate angular velocity (relative
to ITRF2000) and the angular velocity that approximates
the GIA response.

To implement the test, we divided the GPS station ve-
locities into two subnetworks, one consisting of sites that
are located farther than some specified distance from the
approximate center of GIA uplift in North America and the
other consisting of sites within the specified distance. The
distance is treated as an adjustable parameter. The locus of
maximum uplift (called “GIA center” below) is still poorly
constrained, so we approximated it using the location deter-
mined from the assimilation of GPS data into GIA models
by Blewitt et al. (2005, Stable North America Reference
Frame, 55°N - 75°W). Velocities from both subnetworks are
fit via a joint estimation of separate angular velocity vectors
for the two subnetworks. The least-squares fit for the two
subnetwork model is compared to the least-squares fit of a
single angular velocity for the entire data set as follows:

\[
F = \frac{(\chi^2_n - \chi^2_o)/(6 - 3)}{\chi^2_o/(2N - 6)}
\]

where \(N\) is the number of GPS sites used in the esti-
mation, and \(\chi^2_n\) and \(\chi^2_o\) the \(\chi^2\) values for the one network
and two network models, respectively. The significance level
for the observed \(F\) value is compared to that expected for
\(F(3, 2N - 6)\).

Figure 7 shows the probability of the observed improve-
ment in fit calculated from (3) as a function of distance
from the assumed center of GIA uplift. The two-subnetwork
model improves the fit at the 99% confidence level or bet-
ter for all subnetwork geometries with a shared border that
lies within 2100 km of the assumed GIA uplift maximum.
Given that the sites we employ are dominantly located south
of Hudson Bay (Figure 2), the 2100 km cutoff between areas
that are and are not affected by GIA is largely derived from
the numerous velocities in the central and eastern United
States. This cutoff thus does not apply to areas east, west, or north of Hudson Bay, where too few site velocities are found for a meaningful GIA analysis. In Sections 3.2-3.4, we use two techniques to demonstrate the existence and character of the strain gradient associated with GIA at latitudes south of Hudson Bay. Both strongly support the transition to measurable amounts of deformation associated with GIA at distances within 2100-2200 km from the uplift maximum.

Based on the above results, we calculate the North American plate angular velocity with respect to ITRF2000 using sites located at least 2100 km away from the GIA center. Using all the available sites (208 total) yields a reduced $\chi^2$ of 1.7, with a WRMS of 0.9 mm yr$^{-1}$ for both the east and north components. Our best-fitting NOAM/ITRF2000 angular velocity (2.7$^\circ$±0.6$^\circ$, 84.6$^\circ$W±0.2$^\circ$, 0.202±0.002'/Myr; Figure 8) is close to recent values from Altamimi et al. (2002), Beavan et al. (2002), Marquez-Azua and DeMets (2003), and Fernandez et al. (2004).

We inverted subsets of the site velocities with successively smaller standard errors (reflecting sites with longer observation spans and thus presumably better determined velocities). The resulting best-fitting angular velocities do not change significantly, with predicted station velocities in the plate interior that differ by less than 0.2 mm yr$^{-1}$. The entire set of sites located east of 110$^\circ$W and more than 2100 km from the GIA uplift center is thus consistent with the best-fitting angular velocity, including sites with the shortest time series and hence largest uncertainties. For the 119 sites with the best determined velocities, corresponding to those with velocity standard deviations smaller than 1 mm yr$^{-1}$, the WRMS of the residual velocities is 0.7 mm yr$^{-1}$ for the horizontal components.

3.2. Monument stability

Monument stability is a significant issue in the study area because most of the GPS antenna mounts were not designed for tectonic applications. Antennas are mounted on features that range from concrete pillars to fence posts. NGS recently collected information on geodetic monuments at all the CORS sites (G. Sella, pers. comm., 2005). On that basis, we divided the sites in two categories. Category A sites, the monuments that are the most suitable for tectonic applications, consist of monuments installed in bedrock, braced monuments, anchored pillars, or metal rods driven to refusal. Category B sites consist of rooftop monuments and ground monuments that do not belong in Category A such as fence posts, unbraced monuments, masts, and towers.

We assessed monument stability as a function of monument type using two independent measures of monument stability, namely, the magnitude of the random-walk noise present in the detrended individual station coordinate time series (Langbein and Johnson, 1997) and the magnitude of the residual site velocities relative to the best-fitting model predictions (assuming a single rigid plate rotation). The former provides useful information about long-term monument stability and the relative stabilities of differing monument types, independent of plate modeling assumptions. Use of the residual site motions to study monument stability requires an assumption that no internal plate deformation occurs. If empirically-based algorithms for estimating site velocity uncertainties are approximately correct, then a regression of site velocity misfits versus estimated velocity uncertainties should yield a slope of one and intercept of zero. Departures from those values may yield useful insights about the existence of systematic errors in site velocities that are not captured through time series analysis and thus are not incorporated into empirical algorithms for estimating velocity uncertainties.

Random-walk noise was estimated for each site time series using the maximum likelihood estimator (MLE) technique described by Langbein and Johnson (1997). Random-walk noise magnitudes are less than 2 mm yr$^{-1/2}$ (Figure 9A) at more than 90% of category A sites, and never exceed 3 mm yr$^{-1/2}$. In contrast, ~30% of the category B sites exhibit random-walk noise magnitudes greater than 2 mm yr$^{-1/2}$ (Figure 9A), with ~10% of the sites exhibiting values greater than 5 mm/sqrt(yr). Category A sites are also more likely to have smaller residual velocities than are Category B sites (Figure 9B), with ~75% of Category A sites exhibiting residual velocities smaller than 1.2 mm yr$^{-1}$ versus ~60% of Category B sites.

Despite evidence that Category A sites are more likely to have smaller random-walk noise and residual velocities than are Category B sites, no clear correlation emerges between the magnitude of random-walk noise for an individual site and the magnitude of its residual velocity (Figure 10). Although this might imply that systematic sources of noise in monument motion are more important than is random monument wander in causing deviations from rigid plate behavior at individual sites, we instead suspect that the expected correlation will emerge once the measurement time spans among sites get significantly longer than 5 years, the minimum required in order to reliably estimate random-walk noise parameters (Langbein and Johnson, 1997).

If no deformation occurs in a plate interior and monument motion does not include systematic components, which do not average down over time, residual site velocities should decrease as measurement time spans increase due to averaging down of long-period noise. Surprisingly, we find no clear correlation between the misfit magnitudes and observation time spans (Figure 11A), nor do we find a compelling correlation between the misfit magnitudes and velocity uncertainties (Figure 11B). Large velocity misfits (> 2 mm yr$^{-1}$) are found at sites with small velocity uncertainties and long observation spans, even for sites with presumably more stable monumentation.

The lack of evidence for obvious correlations between measurement time span, velocity misfits, and monument quality as measured by monument type and the magnitude of random monument wander is an unexpected outcome of our analysis. One possible explanation for this result is that deviations from the idealized rigid plate motion at a given site may be strongly influenced by systematic noise or noise that occurs at decadal or longer scales, too long to be fully characterized with the present GPS time series. Such noise could arise from geologic or hydrologic processes, could result from long-term site-specific changes in antenna multipath noise, or could be an artifact introduced by one or both of our data processing schemes.

3.3. Residual velocities

Residual velocities with respect to stable North America as defined above are not significant at most sites at the 95% confidence level (Figure 12). They appear to be randomly distributed in direction and magnitude south of about 38$^\circ$N. North of that latitude, however, we observe systematic residual site motions of 0.5-2 mm yr$^{-1}$ toward the south and southeast, particularly at sites in Canada southwest of Hudson Bay and sites in the Great Lakes area, upper Midwest, and New England (Figure 13).

Evidence for the south- to southeastward bias in velocities in these areas is also illustrated by the distribution of residual velocities shown in Figure 14. For the entire study area as well as for sites located more than 2100 km from the GIA center, the residual velocities define a Gaussian distribution centered on a zero-mean residual velocity. Residual velocities at sites located within 2100 km of the GIA center, however, show a deviation from a zero-mean for the north component, consistent with results reported in Section 3.1.
We next use three different techniques to seek spatially coherent patterns within the residual velocities and establish rigorous limits on their geographic extent and strain rates. Previous authors have used the weighted root-mean-square misfit of the angular velocity vector that best-fits their respective North American plate GPS velocity fields to estimate an upper limit for internal plate deformation (e.g., Argus and Gordon, 1996; Dixon et al., 1996; Marquez-Azua and DeMets, 2003), yielding a 95% upper limit of \( \sim 2 \) mm yr\(^{-1}\) on intraplate deformation. Because such estimates reflect the random dispersion of the station velocities with respect to the model predictions, they are of little use for detecting and characterizing the magnitude of any distributed plate deformation, which is likely to be spatially coherent. In contrast, the techniques we employ are designed to extract spatially coherent patterns.

### 3.4. Spatial filtering

If the residual site velocity vectors for locations farther than 2100 km from the GIA center are truly random, then averaging the residual velocities over geographic areas of appropriate size should reduce the averages to values close to zero. Conversely, any regionally coherent patterns in residual velocities should be enhanced via spatial averaging of residual velocities, provided that averaging occurs over appropriately-sized geographic areas. We therefore take advantage of the spatial redundancy in the GPS station velocities by computing regional averages \( v \) using:

\[
v = \frac{1}{\sum_{i=1}^{N} w_i} \sum_{i=1}^{N} w_i v_i(4)
\]

where \( v_i \) are measured GPS velocities and \( w_i \) a weighting function based on an nearest neighbor search scheme defined by:

\[
\sigma_i = \frac{1}{\sigma^2} \times \frac{1}{1 + \frac{r^2}{d_s^2}}(5)
\]

\( \sigma_i \) is the standard deviation of the GPS velocities, \( d \) the distance between GPS sites, and \( d_s \) a given search radius.

We applied this spatial filtering scheme to the residual velocities described above, using search radii \( d_s \) ranging from 100 km to 1000 km. Several interesting patterns emerge from the spatially averaged residual velocity field. Independent of the assumed value for \( d_s \), the residual velocity field is dominated by the pattern of S to SEward trending velocities in Canada and the NE U.S. at rates up to 1.5 mm yr\(^{-1}\) (Figure 15). This confirms the previously described regional coherence of the south- to southeastward residual velocities for sites in the northeastern U.S. and eastern Canada and constitutes a robust long-wavelength feature of the North American GPS velocity field, limited largely to areas within 2100 km of the GIA uplift center. This feature is discussed in Section 3.5.

At distances farther than 2100 km from the GIA uplift center, nearly all of the spatially averaged residual velocities converge to values smaller than 0.5 mm yr\(^{-1}\) for all averaging radii greater than 300 km (Figure 15). This indicates an absence of coherent intraplate deformation at long wavelengths and rates exceeding several tenths of a millimeter per year, thereby defining the nominally undeforming plate interior. Features in the velocity field with wavelengths shorter than several hundred km are severely attenuated by this procedure, thereby necessitating examination of the unfiltered residual velocities for areas such as the New Madrid Seismic Zone, where localized strain may occur (see Section 5).

There are three notable exceptions to a random pattern of residual velocities farther than 2100 km from the GIA uplift center. An east-west belt of north-directed residual velocities with magnitudes of 0.2-0.3 mm yr\(^{-1}\) extends west from Illinois through Iowa, Nebraska, and into Colorado. Similarly slow, but northeast-directed residual site motions are observed in Kansas and Oklahoma. Finally, seaward-directed residual site motions at rates up to 0.4 mm yr\(^{-1}\) are observed in the Gulf Coast states of Florida, Alabama, and Louisiana. These features may result from geophysical processes such as long wavelength effects of GIA or flexural response to sediment loading in the Gulf, or may be an artefact of systematic correlated errors in the GPS analysis. Given the small magnitude of these residuals, longer time series are necessary to further investigate their origin.

### 3.5. Testing Strain Models

#### 3.5.1. Bounds on plate-wide and regional uniform strain

If distributed deformation occurs in the plate interior, as appears to be the case (Figure 15), the raw GPS velocity field (in ITRF2000) should be better fit by a model that includes a strain component in addition to a rigid rotation. Below, we test three hypothetical strain fields: (1) uniform strain in the north-south direction, (2) uniform strain in the east-west direction, and (3) uniform radial strain centered on the GIA maximum. We calculate, for each strain field tested, an \( a priori \) corrections to the raw velocities, then invert the corrected velocities for a best-fitting angular velocity vector. We quantify whether models that include strain and rigid rotation fit the data significantly better than strain free models using an F-test:

\[
F = \frac{(\chi^2_p - \chi^2_f)/(4 - 3)}{\chi^2_p/(2N - 4)}(6)
\]

where \( N \) is the number of GPS sites used in the estimation, and \( \chi^2_p \) and \( \chi^2_f \) the \( \chi^2 \) values for the 3-parameter and 4-parameter models, respectively. The significance level associated with the observed improvement in fit is determined by comparing the observed \( F \) value to that expected for \( F(1, 2N - 4) \).

Figure 16 and Table 2 summarize the results for the uniform east-west, north-south, and radial strain models tested. For all three models and all velocity subsets we considered, the data are inconsistent with uniform strain (shortening or stretching) at rates that exceed \( 10^{-9} \) yr\(^{-1}\). Allowing for uniform north-south strain significantly improves the fit to the entire data set and leads to even more significant improvements in fit for the northeastern U.S. alone, an area than spans the 2100 km divide discussed above. For all stations in the study area, a model that corrects velocities for \( 2 \pm 1 \times 10^{-9} \) yr\(^{-1}\) (95% limit) of north-to-south shortening prior to their inversion for a best-fitting angular velocity vector yields the best fit. The velocities from 63 sites in New England are consistent with the existence of north-south and/or radial shortening at strain rates of \( 8 \pm 2 \times 10^{-10} \) yr\(^{-1}\) (Figure 16). Allowing for strain does not improve the fit, however, when the northern or southern parts of the study area are taken separately. This indicates that the north-to-south shortening that is required by the entire data set is localized along the boundary between the northern and southern domains of the study area, consistent with results reported in Sections 3.2 and 3.3. No similar improvement in the fit occurs when east-west strain is assumed to affect the 220 station velocities from the whole study area. The best-fit strain rate differs insignificantly from zero and the available velocities impose an upper 95% limit of \( 1.5 \times 10^{-10} \) yr\(^{-1}\) on any east-west stretching and an even more severe upper limit of \( 5 \times 10^{-10} \) yr\(^{-1}\) of east-west shortening. For the 3100 km east-to-west width of the study area, these strain rates correspond to maximum integrated velocities of 0.5 mm yr\(^{-1}\) for stretching and 0 mm yr\(^{-1}\) for shortening.

The 0.5 mm yr\(^{-1}\) upper bound on east-west integrated deformation across central North America, corresponding to
a maximum strain rate of $1.5 \times 10^{-10}$ yr$^{-1}$ across the plate interior, is to our knowledge the first estimate that imposes clear bounds on possible patterns of deformation that might be hiding in the North American plate GPS velocity field. Relative to the 2 mm yr$^{-1}$ 95% upper bound estimated for the plate interior by previous authors, the bound we estimate for any east-west deformation is a factor of four smaller. The bounds found here for intraplate strain are consistent with values derived from historical seismicity in the Eastern U.S. ($10^{-12}$ to $10^{-10}$ yr$^{-1}$; Anderson, 1986) and eastern Canada ($10^{-13}$ to $10^{-12}$ yr$^{-1}$; Mazzotti and Adams, 2005).

### 3.5.2. Bounds on strain from GIA

Given that the strongest plate-wide deformation signal is likely to result from GIA, we also tested a radial strain model that simulates GIA deformation as the sum of two Gaussian functions. Horizontal velocities are modeled as:

$$
V_{th} = A_s(e^{-((r-R_c)/W_s)^2} - e^{-((r+R_c)/W_s)^2}) + A_e^{-((r-R_c)/W_e)^2} 
$$

where $r$ is the radial distance to the GIA center, $A_s$ is the magnitude of the maximum positive velocity in the uplift area, $R_c$ is the characteristic distance in the uplift area, $A_e$ the magnitude of the maximum negative velocity in the forebulge, $W_c$ its distance with respect to the GIA center, and $W_e$ the characteristic distance in the forebulge. Similarly, vertical velocities are modeled as

$$
V_{vp} = A_s e^{-(r/W_s)^2} + A_e^{-((r-R_c)/W_e)^2} 
$$

where $A_s$ is the maximum uplift rate, $R_c$ the distance from that maximum to the GIA center, $W_s$ the characteristic decay distance in the uplift area, $A_e$ the maximum subsidence rate, and $W_e$ the characteristic decay distance in the forebulge. This simple geometrical model is obviously not meant to reproduce the physical processes at work, but to test whether the data are consistent with a GIA-like pattern using only 5 (vertical) and 6 (horizontal) parameters, in addition to the 3 rigid rotation parameters. In the search of the best fit parameters, we keep the location of the GIA center fixed to W75°/N55°. The best-fit model parameters are listed in Table ???.

Figures 17 and 19 show that vertical motions are consistent with the lack of resolution imposed by the sparse spatial coverage of continuous GPS stations in Canada. Although earthquake catalogs in North America are limited to ~500 years, they may not be representative of longer time spans, these comparisons provide an external test for the geodetic results presented here. Also, if the intraplate strain detected here is primarily caused by GIA, as we suspect (see also Mazzotti et al., 2005), the GIA contribution to intraplate seismicity, at least in southeastern Canada and northeastern U.S. (Stein et al., 1979, 1989; Hasegawa and Basham, 1989; Wu and Johnston, 2000).

### 3.6. Vertical motions

Figures 17 and 19 show that vertical motions are consistent with a GIA pattern. We find vertical velocities of 10 mm yr$^{-1}$ uplift just east of Hudson Bay, consistent with the location of the GIA center proposed by Blewitt et al. (2005). The maximum uplift rate is however poorly resolved because of the lack of sites near the GIA center. Vertical velocities decay outwards to values of zero (the hinge line) at distances of ~1500 km from the GIA center. Subsidence in the forebulge reaches a maximum of 1.4±0.7 mm yr$^{-1}$ at a distance of 2100 km from the GIA center, consistent with the horizontal velocity profile shown in Figure 17, in which the transition from areas experiencing significant shortening to areas of insignificant strain also occurs at distances of ~2000 km from the center of GIA uplift. That the maximum subsidence in these two triangles encompassing the St Lawrence seismogenic zone are consistent with compressional earthquake focal mechanisms and their NS to NW-SE P-axis (Bent et al., 2003). In addition, we find strain rates in these triangles that are consistent with the lower end of the 1-4$ \times $10$^{-9}$ yr$^{-1}$ rates reported by Mazzotti et al. (2005) in the St Lawrence region on the basis of denser GPS campaign measurements.
4. The New Madrid Seismic Zone

4.1. GPS results

Although our residual velocity field for the central and eastern U.S. shows no obvious pattern of regional-scale strain, the existence of regions of significant localized strain in the central and eastern U.S. has been suggested by several authors. For instance, using a GPS-triangulation comparison, Liu et al. (1992) found a shear strain rate of 0.108±0.045 µrad yr⁻¹ in the southern part of the New Madrid Seismic Zone (NMSZ), corresponding to a slip rate of 5 to 7 mm yr⁻¹. Snay et al. (1994), however, using similar data in the northern part of the NMSZ, found strain rates of 0.03±0.019 µrad yr⁻¹, indistinguishable from zero. Similarly, Weber et al. (1998) and Newman et al. (1999), using GPS data from campaigns performed between 1991 and 1997, found a slip rate of 0.2±2.4 mm yr⁻¹ in the NMSZ. Gan and Prescott (2001) analyzed GPS data from continuous GPS stations in the central and eastern U.S. and argue for significant deviations from rigid plate behavior in the Mississippi embayment, which they interpret as evidence for elevated strain rates. More recently, Smalley et al. (2005) propose that relative motions between CGPS sites in the NMSZ are significant and comparable to deformation rates along active plate boundaries.

Our results show no detectable residual motion in the NMSZ at the 95% confidence level (Figure 20). The average weighted residual for sites in the region with respect to the predictions of our best-fitting North American plate angular velocity vector is 0.7 mm yr⁻¹, comparable to that for sites outside the region. None of the individual site velocities are significant at the 95% confidence level.

A key question is whether the apparent shortening of 1.6±1.2 mm yr⁻¹ (68% confidence) between sites RLAP and NWCC across the Reelfoot fault is significant, as recently proposed by Smalley et al. (2005). An examination of the baseline time series between these two sites (Figure 21) suggests that the apparent shortening is not caused by a linear decrease in the inter-station distance, as might be expected if the cause of the shortening was tectonic, but is instead a result of an 8 mm offset between 2001 and 2002 that separates two periods of no discernible change in the baseline length. The offset, which originated at site NWCC, does not correspond to any equipment changes, significant earthquakes, or known creep events at or near site NWCC and is thus difficult to explain. Whatever the explanation, the apparent shortening between RLAP and NWCC reported here as well as by Smalley et al. (2005) results from this unexplained offset and is unlikely to represent steady, long-term strain accumulation on the intervening Reelfoot fault.

4.2. Implications for earthquake recurrence

Based on our 0.7 mm yr⁻¹ weighted RMS value for the residual velocities of the NMSZ sites, random deviations from a rigid plate model in the NMSZ region do not exceed 1.4 mm yr⁻¹ at the 95% confidence level. We assume that this represents a conservative upper bound on the magnitude of any long-term slip in the study area. Assuming a simple model where characteristic earthquakes repeat regularly on a given active fault – as is implicit in the U.S. earthquake hazard maps, for instance – our results imply a minimum repeat time of about 3,000 to 8,000 years for future magnitude 8 earthquakes with 5-10 m of coseismic slip (Figure 22). For comparison, National Seismic Hazard Maps (Frankel, 1996) assume a 1,000 year recurrence time for M8 events with 5 m of coseismic slip. The implied ~5 mm yr⁻¹ of long term slip rate on the New Madrid faults is a factor of four faster than the upper bound suggested by our analysis.

Similarly, our 1.4 mm yr⁻¹ upper bound implies a minimum repeat time of 600-1,500 years for future magnitude 7 earthquakes with 1-2 m of coseismic slip (Figure 22). This is consistent with recent and historic earthquake catalogs, which predict a recurrence interval that exceeds 1000 years for magnitude 7 earthquakes, and 10,000 years for magnitude 8 earthquakes (Newman et al., 1999) on several consistent with paleoseismic data (Kelson et al., 1994; Tuttle and Schweig, 1995; Tuttle et al., 1999), which imply recurrence intervals of 400 to 1,000 years.

5. Conclusions

Our analysis of data from more than 300 continuous GPS sites in the North American plate interior indicates that the velocity field is described within uncertainties by a simple rigid plate rotation that is modified in some areas by a deformation pattern consistent with glacial isostatic rebound. After correcting the individual GPS station velocities for the predicted motion of the North American plate, residual horizontal velocities reach ~0.8 mm yr⁻¹ close to the GIA center and decrease outward in a quasi-radial pattern. Analysis of the residual velocity field reveals a significant, north-to-south deformation gradient of ~1 mm yr⁻¹, primarily localized between 1000 and 2200 km from the GIA center and corresponding to strain rates of about 10⁻⁹ yr⁻¹. At distances farther than 2100 km from the GIA center, horizontal residual velocities are random and exhibit no evidence for regions of elevated strain rates. In particular, we find no detectable residual motion at the 95% confidence level in the New Madrid Seismic Zone, where the average weighted misfit of 0.7 mm yr⁻¹ is the same as the weighted misfit of our rigid plate model. The numerous velocities impose severe upper (95%) bounds of 1.5 x 10⁻¹⁰ yr⁻¹ on east-west uniform strain rates in eastern and central North America. The implied, integrated deformation rate across the plate interior is less than 0.5 mm yr⁻¹, a factor of four smaller than upper bounds estimated by previous authors.

Our results compare well with those reported for other plate interiors. In Western Europe, magnitude 7 paleo-earthquakes are inferred in the Rhine graben, but no surface deformation has yet been resolved with GPS at the 0.8 mm yr⁻¹ level (Nocquet et al., 2005). GPS measurements in Australia also show no deformation within their 0.8 mm yr⁻¹ resolution (Beavan et al., 2002), despite several significant earthquakes in the past two decades. Although the instrumental and paleoseismological record of intraplate earthquakes indicates that tectonic stresses within plate interiors accumulate on faults and are released during large infrequent events, geodetic observations on several major plates have not yet been able to resolve the associated surface deformation. Interseismic strain loading of faults in plate interiors may thus be smaller than the present GPS detection threshold, or strain accumulation may occur mostly at depth through transient processes that may have little to no surface signature, as proposed by Kenner and Segall (2000) for the New Madrid area.

Our results reveal the existence of significant horizontal and vertical deformation associated with glacial isostatic adjustment, extending as far as 2100 km from the assumed center of GIA uplift just east of Hudson Bay. Although a rigorous comparison of the 3-D deformation constraints that our residual velocities impose on GIA deformation is beyond the scope of this paper, a first-order comparison with the predictions of the VM1 and VM2 end-member models described by Petitter (1998) suggests that model VM1 is more consistent with the observed absence of any GIA effects south of 40°N (Figure 15) than is model VM2. In this regard, our results agree with conclusions reached by Argus et al. (1999) regarding the superior compatibility of the predictions of model VM1 with the very long baseline interferometry and satellite laser ranging geodetic constraints they present.
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References


E. Calais, Purdue University, Department of Earth and Atmospheric Sciences, West Lafayette, IN 47907, USA (ecalais@purdue.edu)

J.Y. Han, Purdue University, Department of Geomatics, West Lafayette, IN 47907, USA (han5@purdue.edu)

C. DeMets, University of Wisconsin, Department of Geology and Geophysics, Madison, WI 53706, USA (chuck@geology.wisc.edu)

J.M. Nocquet, Centre National de la Recherche Scientifique, UMR6526 Geosciences Azur, 250 Rue A. Einstein, 06560 Valbonne, France (nocquet@geoazur.unice.fr)
Figure 1. Topography and seismicity in the midcontinent. Limited to earthquakes with magnitudes greater than 3 in the National Earthquake Information Center PDE (1973-Present) and Significant U.S. Earthquake catalogs (1568-1989).
Figure 2. Map of continuous GPS stations used in this study. Symbol colors specify length of observation time series.
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Figure 16. $\chi^2$ as a function of strain rate for a series of models that include rigid rotation and strain (explanations in the text). The horizontal lines shows the 95% confidence level for each model tested. Positive strain rates indicate extension; negative indicate compression. The northeastern U.S. (bottom right) comprises sites from 35°N–43°N and 85°W–75°W.
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Figure 20. Residual velocities in the NMSZ. The individual GAMIT and GIPSY solutions are shown together with the combined solution and the velocities published by Smalley et al. (2005). Seismicity is from the CERI catalog.
Figure 21. NWCC-RLAP baseline length time series (weekly solutions).
Figure 22. Recurrence time for M7 and M8 earthquakes, with two end-member values of coseismic slip for each magnitude (after Newman et al., 1999). NSH = National Seismic Hazard maps. Paleoseismology is from Tuttle and Schweig (1995).
<table>
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<tr>
<th>solution</th>
<th>a posteriori variance factor</th>
<th>Position WRMS in mm</th>
<th>Velocity WRMS in mm/yr</th>
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</thead>
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<td>2.4</td>
<td>0.8</td>
<td>5.2</td>
</tr>
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<td></td>
<td></td>
<td>0.5</td>
<td>2.0</td>
</tr>
<tr>
<td>GIPSY</td>
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<td>1.8</td>
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<tr>
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<td></td>
<td>0.2</td>
<td>0.5</td>
</tr>
<tr>
<td>IGS</td>
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<td>5.9</td>
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<td>3.5</td>
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<tr>
<td></td>
<td></td>
<td>0.4</td>
<td>0.7</td>
</tr>
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</table>

Table 1. Statistics of the combination.
Table 2. Statistical tests for significance of best intraplate strain models. Numbers express the probability that the GPS station velocities from the stated geographic areas are consistent with zero strain rate within their uncertainties. Probability is determined using an F-ratio test that compares the least-squares misfits to the station velocities for zero strain rate (e.g., no deformation of the plate interior) to the strain rate that allows for the best least-squares fit to the velocities for an assumed strain model. Probabilities take on values from 0-100%, with smaller values corresponding to increasingly low probabilities that the data are consistent with a rigid plate interior.

<table>
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<tr>
<th>Strain model</th>
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<th>&gt; 40°N</th>
<th>NE U.S.</th>
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<tbody>
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<td>63</td>
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<td>65%</td>
<td>100%</td>
<td>10%</td>
<td>22%</td>
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<tr>
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<td></td>
<td>0.1%</td>
<td>68%</td>
<td>10%</td>
<td>0.03%</td>
</tr>
<tr>
<td>Uniform strain centered on GIA maximum</td>
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<td>16%</td>
<td>100%</td>
<td>100%</td>
<td>0.004%</td>
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